Studies on Closed-loop Interaction in a Multi-loop Single Tank Control System

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Abstract

This paper investigates the interaction between level and flow loop in a single tank system. The data generated is used to generate all transfer functions via step test method. The model generated is then simulated on MATLAB-Simulink and the obtained results are then compared with experimental results for verification. A Relative Gain Array analysis is performed to check the interaction and comment on the pairing.

Keywords: MIMO Process; Relative Gain Array; Step Test Method; Simulink

1. Introduction

A MIMO is a process in which there are multiple inputs and multiple outputs and each one of them can influence the other. Most of the industrial processes in chemical industry revolve around multi-input, multi-output process which cannot be understood with the principles established for single-input, single output process. The problem with process control of MIMO processes is the interaction between loops and how to regulate them. A MIMO process due to interactions between different inputs and outputs raises the question of pairing of each of these processes variable to each other so that we get a process with least interaction and highest stability (Liu, Zhang, and Gu, 2005). To control a MIMO process a generalized approach in the industry is to use \( n \) PI or PID controllers for \( n \) control variables (Gagnepain and Seborg, 1982). Given this approach is so widely used in industry, we will also design our experiment according to this heuristic. To study a multi-loop control system, we designed a single tank system with level and flow loop on a Universal Process Trainer. A Universal process control trainer helps understand the process control of various industrial systems by providing us with different tools which include control valves, controllers for different variables, variable transmitters and many other instruments which help us to study different systems generally seen in an industrial unit (Apex 2012).

2. Analysis and Design

A. Block Diagram Analysis

Block diagram analysis compacts all the gain functions of a process in a matrix. For a MIMO process, this tool helps in the analysis of gain function of respective loops and disturbance from interactions between loops. A 2\( \times \)2 MIMO process will have four gain functions as represented in the figure below. Figure 1 shows a process which is on 1-1/2-2 controller setting. Our system will be configuring for 1-1/2-2 controller setting. There is an alternate pairing scheme too known as 1-2/2-1 controller setting. In this setting input 1 is controlling output 2 and input controlling output 1 as shown in Figure 2.

B. Ziegler Nicholas Tuning Method

PID controllers are the most widely used controller in industry. A common heuristic approach in tuning these controllers is Ziegler Nicholas method (Acosta, Mayosky, and Catalfo, 1994). This heuristic is only applied when the system is in closed configuration. A brief summary of the process as given in the original paper (Ziegler and Nichols, 1993):

1. Turn off the derivative and integral action of the controller.
2. Increase the proportional control from zero till the process reaches a quasi-static state.
3. Note down the critical gain and critical time period.
4. Use the Z-N table to tune your controller.

As an accepted heuristic, this method was used in the experimental setup to tune the PIDs of both controllers. Although Z-N heuristic is not the most reliable method for tuning of PID controller (Acosta et al., 1994) it did give acceptable results and further tweaking improved the action of both the controllers.

C. Relative Gain Array Method

Pairing and interaction are the two most important questions in a MIMO process. Bristol in 1966 developed a systemic approach...
called Relative Gain Array Method to answer these questions (McAvoy et al., 2001). This method relied on the concept of relative gain. Bristol considered a process with \( n \) controlled variables and \( n \) manipulated variables, relative gain \( \lambda_{ij} \) was defined as gain between a controlled variable, \( Y_i \), and manipulated variable, \( U_j \) which equals steady state gain of process in two states (Seborg et al., 2004).

\[
\lambda_{ij} = \frac{\left( \frac{\partial Y_i}{\partial U_j} \right)_{U_i=0}}{\left( \frac{\partial Y_i}{\partial U_j} \right)_{U_i=0}} = \frac{\text{open-loop gain}}{\text{closed-loop gain}}
\]

(1)

Assume a 2 x 2 process with \( u \) as input and \( y \) as output. RGA of this process will be:

\[
\Lambda = \begin{bmatrix}
\lambda & 1 - \lambda \\
1 - \lambda & \lambda
\end{bmatrix}
\]

(2)

where,

\[
\lambda = \frac{1}{1 - \kappa k_{22} k_{12}}
\]

(3)

where, \( \kappa \) is steady state gain.

According to the calculated value of \( \lambda \) comments are made about the interaction between loops as described in Table 1.

<table>
<thead>
<tr>
<th>Value of ( \lambda )</th>
<th>Recommended Configuration</th>
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<tbody>
<tr>
<td>( \lambda \geq 0.5 )</td>
<td>1-1/2-2 configuration</td>
</tr>
<tr>
<td>( \lambda &lt; 0.5 )</td>
<td>1-2/2-1 configuration</td>
</tr>
</tbody>
</table>

### 3. Experiments, Results and Discussion

#### A. Stability of loop response after Z-N Tuning

Both the controllers were tuned using Z-N tuning analysis. Although response curves were still not stable after tuning, the values obtained from Z-N tuning were modified till stable response curves were required for both loops as shown in Fig. 3 and 4.

#### B. Interaction Experiments

After tuning of controllers, interaction experiments were performed to confirm interaction between loops as shown in Fig. 5 and 6.

#### C. Step Test and Transfer Functions

Step Test was performed on both the loops in open loop configuration. Graphical analysis is shown in Fig. 3 and Fig. 4.
D. Transfer Functions

\[ G_{p1} = \frac{1.5e^{-1.5s}}{7s + 1} \]
\[ G_{p2} = -\frac{0.08e^{-0.75s}}{5s + 1} \]
\[ G_{p21} = -\frac{0.21e^{-3s}}{6s + 1} \]
\[ G_{p22} = \frac{0.8e^{-0.08s}}{6s + 1} \]
G. Discussion

The following points discuss the result obtained:

1. Model generated predicts correctly the nature of response for a given step change but is not precise with quantification of the response generated in the loop.
2. The model generated is a linearized approximation of the experimental setup and this might be the reason for the incorrect prediction of amplitude of response.
3. RGA analysis of the setup suggests a 1-1/2-2 configuration for the least interaction setup which is already followed.

4. Conclusion

We can conclude from our set of experiments and discussion that linearized model of a level-flow multi-loop system although predicts the nature of response, can be improved for quantitative predictions and 1-1/2-2 configuration gives the least interaction pairing of a level-flow multi-loop system.

References


