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Research paper



A Study on Model Aircraft F1A Glider Glide Performance According to Airfoil

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Abstract

The objective of this study was to investigate the effect of airfoil difference of F1A glider on gliding flight sink rate of model aircraft for improving competition score of F1A glider and providing basic data necessary for the development of model aircraft in Korea. Altitude Reached, set time, and sink rate were measured for a model aircraft of conventional airfoil with a large under camber and low airfoil (LDA) concept aircraft. Model aircraft of airfoil with a large under camber and model aircraft of airfoil with a large under camber and model aircraft of airfoil with a large under camber and low airfoil) concept were constructed. They flew twice each at Osom airfield in Hwasung city, Gyeonggi province, Korea under zero wind condition. After comparing the lift-to-drag ratio of lift coefficient and drag coefficient for the angle of attack, an altimeter was installed in each model aircraft. After each flight, data of each model were analyzed and sink rate with altitude was compared. All data were analyzed using SPSS version 18.0 for Windows. Mean (M) and standard deviation (SD) were calculated. Independent sample t-test was performed to determine inter-group difference. Statistical significance level was set at p < 0.05. Results of this study were as follows. First, the optimized lift-to-drag ratio according to angle of attack was obtained through airfoil data analysis. Second, flight altitude and sink rate were determined. Third, through data analyses, a more scientific approach was made possible for competition operation.

Keywords: Aeromodelling, Aircraft, Glider, Airfoil, Angle of Attack, Sink Rate

1. Introduction

Model aircraft, a kind of aviation sport, is operated by the pilot operating the model aircraft. It is the most representative of aviation sports with a very fast development in the history of aviation sports worldwide.

Model aircraft plays a role in the backdrop of increasing number of people participating in aviation sports in their leisure time as one characteristic of the modern society which has reached an era of leisure. It has the longest history in aviation sports with many club members (about 100,000 people nationwide). Presidential, Air Force Chief of Staff, and Minister of Land, Transport, and Maritime host competition annually and around 1,000 people attend each competition. It is the most important sporting event in aviation sports fields considering the number of club members and competitors [1].

Model aircraft is defined by the Sporting Code of the Fédération Aéronautique Internationale (FAI) currently used by about 100 countries. The Fédération Aéronautique Internationale (FAI) has 11 CIAM subcommittees, including model aircraft. There are 12 subcommittees in the model aircraft category, including free flying events. It is also made up of national NAC (National Air Sport Controls) [2]. In Korea, NAC is the Federation of Korea Aeronautics (KFA) and the Korea Aero Models Association (KAMA) is an affiliate organization that promotes and encourages this hobby of clubs, supports air experience classes in elementary, junior high, and high schools, organizes and hosts national competitions. Once every two years, national athletes from each sport are selected and given the opportunity to participate in FAI-sponsored world championships [3].

Free Flight category as one of model aircraft categories does not operate externally like RC planes or drones. It is designed to be stabilized by a combination of settings such as flight shape, center of gravity, and attachment angle of main wing and tail wing even when flying becomes unstable due to gusts or rising airflow during flight.

F1A glider category, a free-flying category, was also known as Nordic A / 2 before the Fédération Aéronautique Internationale (FAI) enacted in 1948. It was based on model glider specifications made by Sweden and Finland in the 1940s [4]. As of November 2016, FAI has many athletes and clubs around the world. There are about 600 registered competitors on the ranking that lists only international athletes with good scores.

Although 60 years have passed since the 1951 World Championships in Yugoslavia with various international competitions on the way, restricted regulations of wing area of $32 \sim 34$ dm2, weight of 410 g or more, and pull string tension of 5 kg with less than 50 m remain unchanged. Since world championships, various international competitions, and domestic official competitions are conducted in such a manner that the set time after launching the flight body is summed in each round and ranked, it is necessary to ensure high altitude and efficient gliding design with gliding flight before starting gliding flight to obtain good results in the restricted range.



F1A glider flies in a circle to detect ascending airflow during flight. If an ascending air current is detected, the athlete will run to make a departure and the airframe accelerated at high speed is separated from the hook having a tensile strength of 12 kg or more, which is 30 times the minimum airframe weight of 410 g. When the bunt is done, it rises to an altitude of 20 m or more than the tow line length and then starts a gliding flight. Because it is an endurance flight game, it uses airfoil with a large under camber that is hard to see on practical or RC airplanes as it is only pursuing the lowest sink rate when flying. Compared to main wings made of D-BOX structure manufactured by using blast furnace until 1987 (in 1988, the strength of the main wing and horizontal tail wing of the D-BOX structure made of composite material became stronger), the maximum thickness of 9 mm (6%) was developed based on the main wing airfoil prototype 150 mm [5]. Although airfoil with large under camber has the advantage of low sink rate in gliding flight, it has disadvantage in that it does not acquire high altitude due to large drag at the moment of bunting after accelerating in tow flight.

To compensate for the disadvantage of airfoil with a large under camber, world champion Roland Koglot used an airfoil with the concept of LDA (low-drag airfoil) and compared to existing airfoil with a large under camber. The gliding flight starts at an altitude of about 80 m to 110 m after rising from the tow line to 30 m \sim 60 m. It became a necessary condition to win the competition by attaining an altitude through the bunt after a sudden acceleration as athletes participating in each tournament are becoming significantly better.

Although the importance of airfoil has been raised to achieve good results in F1A glider race, there have been few studies using scientific approach. Therefore, the purpose of this study was to investigate the sink rate of gliding flight according to the altitude through pilot flight after constructing airfoil glider with the concept of airfoil and LDA (low-drag airfoil). It will provide basic data necessary to improve F1A glider competition scores. This study aims to improve the competition score of F1A glider by investigating the influence of airfoil difference of glider flight on glide flight rate. Results of this study will provide basic data necessary for the development of model aircraft in Korea.

2. Contents and Methods

2.1. Subjects

Subjects of this study were model aircrafts of airfoil with a large under camber and those of airfoil with LDA (low-drag airfoil) concept.

2.2. Experimental Tools and Methods

Altitude acquisition, set time, and sink rate of airfoil and airfoil glider of the concept of airfoil and LDA (low-drag airfoil) were measured. The experiment was conducted at Osom Airfield, Hwaseong City, Gyeonggi Province, Korea. Aircrafts of airfoil with large under camber and LDA (low-drag airfoil) concept airfoil glider were made. They flew twice in zero wind condition. An altimeter was mounted on the selected airfoil. A F1A glider national competitor flew twice with each model after confirming the no-wind condition at Osom Airfield in Songsan-myeon, Gyeonggi-do province, Korea. Data of each model were analyzed. Lift coefficient, drag coefficient, and lift-to-drag ratio for the angle of attack were compared and analyzed for sink rate according to altitude after the flight.

2.3. Data Processing

All data obtained from this experiment were analyzed with SPSS version 18.0 for Windows. Mean (M) and standard deviation (SD) were calculated to provide descriptive statistics of all dependent variables. Independent sample t-test was used to determine intergroup measurements. Statistical significance level was set at p < 0.05.

3. Main Subjects

3.1. Airfoil Selection

An important issue in determining F1A glider glide performance is airfoil selection. For the selection of the most suitable airfoil, airfoil used by participating athletes was selected. Makarov was selected as the airfoil with the large under camber, BE6356, while the airfoil with the concept of LDA (low-drag airfoil) was selected as MID-101 and MID-103. In this study, airfoil with the highest lift-drag ratio (Cl/Cd) will be determined through aerodynamic analysis by using profili2.

3.1.1 Makarov

The shape of Makarov, an airfoil with a large under camber, is as follows.

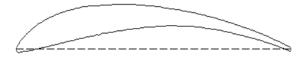


Fig. 1: Two-dimensional cross-sectional shape of Makarov airfoil.

This airfoil, Makarov, has Max thickness 6.40% at 21.4% of the chord and Max camber 6.78% at 48.7% of the chord.

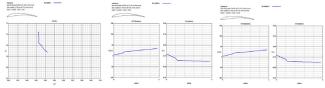


Fig.2: Analysis graph of Makarov airfoil.

Table 1: Analysis results of Makarov airfoil.

Maka	rov-Re=4		1111y 515 103	, uno 01 111	unuro i un		
Al-	Cl	Cd	Cl/Cd	Cm	T Xtr	B Xtr	Power
fa							F.
0.0	0.184	0.042	4.3491	-	0.902	0.076	1.8676
	4	4		0.081	9		
				8			
0.2	0.240	0.040	5.9629	-	0.896	0.073	2.9267
	9	4		0.088		3	
				6			
0.4	0.310	0.038	8.0284	-	0.890	0.071	4.4751
	7	7		0.097	9	7	
				7			
0.6	0.378	0.037	10.131	-	0.884	0.072	6.2361
	9	4		0.106	8	3	
				5			
0.8	0.430	0.036	11.8	-	0.875	0.080	7.7441
	7	5		0.112	3	9	
				4			
1.0	0.493	0.035	13.859	-	0.868	0.115	9.7353
	4	6	6	0.120		1	
				6			
1.2	0.615	0.032	19.003	-	0.868	1.000	14.911
	7	4	1	0.140	9	0	1
				2			
1.4	0.654	0.032	20.197	-	0.860	1.000	16.338
	4	4	5	0.142	8	0	8
				7			
1.6	0.672	0.032	20.574	-	0.846	1.000	16.876

	8	7	9	0.142	6	0	5	BED Tochonal (N. et 22 Tochonal (N. et 22) Tochonal (N. et 22) Tochonal (N. et 22)	iz 400 +	BCNI to horses The canter - 100	In the all contractions of the second		BOX Re Norma 5 1% at 32% of the churd Re Lamber 23% of 32% of the churd Rech + 1002 - 104 - 101	ir 600+	
1.8	0.706	0.032	21.590	-	0.836	1.000	18.140			C					Autor
1.0	0.700	7	21.590	0.143	7	0	9	1	006		Cijene 69	Colene	19	u	
		,	-	8	,	Ŭ		u	1				59	19	
2.0	0.736	0.032	22.532	-	0.827	1.000	19.340		ξ						
	8	7	1	0.145	5	0	9	0		65	6.8 (d		0154		
2.2	0.756	0.033	22.921	-	0.813	1.000	19.934	EE						45	
	4		2	0.144	4	0	9	45							
				7											
2.4	0.791	0.032	24.131	-	0.805	1.000	21.468	tall day	ND ND NH NK NN Cd	10 00 00 00 1	E B	alite a	40		5
	5	8	1	0.146	4	0	5			Fig. 4: An	alysis grapl	n of BE63	56 airfoil		
				3						0					
2.6	0.810	0.033	24.498	-	0.791	1.000	22.060			Table 2: Ai	nalysis resu	lts of BE6	5356 airfo	il.	
	9	1	5	0.145	7	0	9		856-Re=4						
2.0	0.040	0.022	25.520	9	0.700	1.000	22.400	Al-	Cl	Cd	Cl/Cd	Cm	T Xtr	B Xtr	Pow-
2.8	0.840 2	0.032	25.538	- 0.146	0.780 6	1.000	23.408 7	fa							er F.
	2	9		5	0	0		0.0	0.599	0.0278	21.568	-	0.853	0.222	16.70
3.0	0.879	0.032	27.226		0.773	1.000	25.531		6		3	0.134	2	2	12
5.0	4	3	27.220	0.148	8	0	5	0.2	0.(2)	0.0274	22.070	2	0.041	0.242	10.11
		5		3	0	Ŭ	5	0.2	0.626 9	0.0274	22.879	-	0.841 8	0.243 9	18.11
3.2	0.891	0.032	27.091	-	0.756	1.000	25.576		9		6	0.134 8	8	9	54
	3	9	2	0.146		0	4	0.4	0.654	0.0268	24.414	0	0.829	0.308	19.74
				7				0.4	3	0.0208	24.414	0.135	9	5	83
3.4	0.927	0.032	28.623	-	0.747	1.000	27.564		5		2	6		5	05
	4	4	5	0.148	5	0	8	0.6	0.679	0.0252	26.956	-	0.821	1.000	22.21
3.6	0.944	0.032	28.804	-	0.732	1.000	27.998		3		3	0.134	3	0	73
	8	8	9	0.147	6	0	6					9			
				2		1		0.8	0.697	0.0256	27.226	-	0.805	1.000	22.73
3.8	0.975	0.032	29.923	-	0.721	1.000	29.554		0		6	0.134	7	0	05
	5	6	3	0.147 9	6	0	5	1.0	0.725	0.0256	28.328	-	0.795	1.000	24.12
4.0	1.008	0.032	31.229	9	0.712	1.000	31.364		2		1	0.134	6	0	39
4.0	1.008	0.032	1	0.149	0.712 4	0	7					3	. =	4	
	/	5	1	1	7	U	'	1.2	0.744	0.0260	28.638	-	0.781	1.000	24.71
4.2	1.025	0.032	31.274	-	0.697	1.000	31.675		6		5	0.133 7	8	0	22
1.2	8	8	4	0.148	3	0	3	1.4	0.769	0.0261	29.475	/	0.770	1.000	25.85
	-	-		1	-	-	-	1.4	0.709	0.0201	29.473	0.133	3	0	25.85
4.4	1.067	0.032	33.346	-0.15	0.688	1.000	34.447		3		1	5	3	0	23
	1		9		3	0	5	1.6	0.791	0.0263	30.110	-	0.758	1.000	26.79
4.6	1.079	0.032	33.012	-	0.671	1.000	34.299	1.0	9	0.0205	3	0.133	6	0	48
	5	7	2	0.148	2	0	4		-		5	1	0	v	
				4				1.8	0.812	0.0265	30.667	-	0.745	1.000	27.64
4.8	1.115	0.032	34.868	-	0.659	1.000	36.832		7		9	0.132	3	0	71
	8	0	8	0.149	7	0	4					6			
			adunamia	4		1.1		2.0	0.839	0.0264	31.810	-	0.736	1.000	29.15
A c c	hours	OVA DOP	odunamia	charact	rictice o	round th	a airtail					0.100	_	0	

As shown above, aerodynamic characteristics around the airfoil when the angle of attack varied from 0° to 5° in 0.2° increments at Re = 40000 were analyzed. The optimal angle of attack was 3° when the lift ratio (Cl) and the drag coefficient (Cd) were compared

3.1.2 BE6356

The shape of BE6356, an airfoil with a large under camber, is as follows.



Fig. 3: Two-dimensional cross-section of BE6356 airfoil.

The airfoil BE6356 was characterized to have a maximum thickness of 6.10% at 20.2% of the chord and a maximum camber of 6.29% at 36.2% of the chord.

9.74 83 2.21 73 2.73 05 4.12 39 4.71 22 5.85 25 6.79 48 7.64 71 9.15 8 6 0.132 7 0 14 4 0.721 31.572 0.0271 29.20 2.2 0.855 1.000 0 0.131 0 0 36 6 6 32.618 0.711 2.4 0.880 0.0270 1.000 30.61 -0.131 7 5 2 0 11 2.6 0.89 0.027 0.697 1.000 30.9651 84 5 32.669 0.130 2 0 4 1 0.92 2.8 0.027 33.380 0.686 1.000 32.0400 0.129 13 6 4 0 1 8 0.028 0.674 32.6370 3.0 0.94 33.632 1.000 17 0 1 0.129 5 0 2 33.2027 3.2 0.96 0.028 33.859 0.661 1.000 0.128 16 4 2 7 0 6 34.6384 3.4 0.98 0.028 34.869 0.652 1.000 68 3 3 0.128 9 0 0 0.029 34.429 0.637 1.000 34.4622 3.6 1.00 0.127 19 1 6 7 0 3 0.627 3.8 1.02 0.029 35.116 1.000 35.5596 0.126 54 2 4 7 0 6 4.0 1.04 0.029 34.866 0.614 1.000 35.5994 -

25 9 2 0.126 8 0	
0	
4.2 1.06 0.030 35.085 - 0.603 1.000 36.17	58
31 3 8 0.125 3 0	2.
3	
4.4 1.08 0.030 35.316 - 0.592 1.000 36.77	27
42 7 0 0.124 9 0	2.
6	
4.6 1.10 0.031 34.936 - 0.579 1.000 36.65	00
05 5 5 0.123 5 0	2.
9	
4.8 1.12 0.031 35.560 - 0.270 1.000 37.69	54
37 6 1 0.123 4 0	2.
3	

As shown above, aerodynamic characteristics around the airfoil when the angle of attack varied from 0° to 5° in 0.2° increments at Re = 40000 were analyzed. The optimal angle of attack was 3° when the lift ratio (Cl) and the drag coefficient (Cd) were compared and the load ratio (Cl / Cd) was analyzed. The optimum lift-drag ratio (Cl/Cd) is 33.6321.

3.1.3 MID-101

The shape of MID-101, an airfoil of LDA (low-drag airfoil) concept, is as follows.



Fig. 5: Two-Dimensional Cross Section of MID-101 Airfoil.

This airfoil, MID-101, has Max thickness 7.70% at 19.4% of the chord and Max camber 4.50% at 52.4% of the chord.

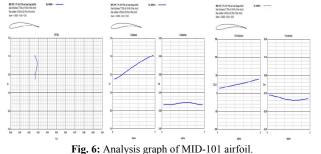


 Table 3: Analysis results of MID-101 airfoil.

MID 101-Re=40000Al- faClCdCl/CdCmT XtrB XtrPower F.0.2 0.369 5 0.026 5 13.943 4 0.110 0 0.000 0.577 3 8.4757 0.4 0.388 7 0.026 7 14.558 1 0.110 3 1.000 0 0.601 2 9.0763 0.6 0.412 9 0.026 9 15.349 4 0.111 5 0.996 6 0.629 8 9.8631 0.8 0.450 8 0.026 9 16.758 4 0.115 0 0.988 1 0.673 4 11.251 81.0 0.479 1 0.026 6 18.011 2 0.116 0 0.977 4 0.738 9 12.466 91.2 0.510 5 0.026 5 19.264 2 0.119 0 0.963 5 1.000 1 13.764 11.4 0.545 3 0.027 4 20.214 8 0.122 0 0.951 0 1.000 4 14.934 41.6 0.582 3 0.027 4 21.251 8 0.125 0 0.939 0 1.000 0 16.217 0	Table 3: Analysis results of MID-101 airfoil.							
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	MID	101-Re=4	0000					
0.2 5 5 4 0.110 0 3 $8.4/57$ 0.4 0.388 0.026 14.558 $\overline{0.110}$ 1.000 0.601 9.0763 0.6 0.412 0.026 15.349 $\overline{0.111}$ 0.996 0.629 9.0763 0.6 9.9 9 4 $\overline{0.111}$ 0.996 0.629 9.8631 0.8 0.450 0.026 16.758 $\overline{0.115}$ 0.988 0.673 11.251 0.8 0.450 0.026 18.011 $\overline{0.116}$ 0.977 0.738 12.466 1.0 0.479 0.026 19.264 $\overline{0.119}$ 0.963 1.000 13.764 1.2 0.510 0.027 20.214 $\overline{0.122}$ 20.951 1.000 14.934 1.4 0.545 0.027 21.251 $\overline{0.125}$ 0.939 1.000 14.934 1.6 0.582 0.027 21.251 $\overline{0.125}$ 0.939 1.000 16.217 <td></td> <td>Cl</td> <td>Cd</td> <td>Cl/Cd</td> <td>Cm</td> <td>T Xtr</td> <td>B Xtr</td> <td></td>		Cl	Cd	Cl/Cd	Cm	T Xtr	B Xtr	
0.4 7 7 1 0.110 0 2 9.0763 0.6 0.412 0.026 15.349 -111 0.996 0.629 9.8631 0.8 0.450 0.026 16.758 -0.115 0.988 0.673 11.251 0.8 0.450 0.026 16.758 -0.115 0.988 0.673 11.251 1.0 0.479 0.026 18.011 -0.116 0.977 0.738 12.466 1.2 0.510 0.026 19.264 -0.119 0.963 1.000 13.764 1.4 0.545 0.027 20.214 0.122 0.951 1.000 14.934 1.4 0.582 0.027 21.251 -0.125 0.939 1.000 16.217 1.6 3.3 4 $8.$ 0.125 0.939 1.000 16.217	0.2							8.4757
0.6 9 9 4 0.111 6 8 9.8631 0.8 0.450 0.026 16.758 $\overline{0.115}$ 0.988 0.673 11.251 0.8 8 9 4 0.115 0.988 0.673 11.251 1.0 0.479 0.026 18.011 $\overline{0.116}$ 0.977 0.738 12.466 1.2 0.510 0.026 19.264 $\overline{0.119}$ 0.963 1.000 13.764 1.4 0.545 0.027 20.214 $\overline{0.122}$ 0.951 1.000 14.934 1.4 0.582 0.027 21.251 $\overline{0.125}$ 0.939 1.000 14.934 1.6 0.582 0.027 21.251 $\overline{0.125}$ 0.939 1.000 16.217	0.4							9.0763
0.8 8 9 4 0.115 1 4 8 1.0 0.479 0.026 18.011 $ 0.977$ 0.738 12.466 1.2 0.510 0.026 19.264 $ 0.963$ 1.000 13.764 1.4 0.545 0.027 20.214 $ 0.951$ 1.000 14.934 1.4 0.582 0.027 21.251 $ 0.939$ 1.000 14.934 1.6 0.582 0.027 21.251 $ 0.939$ 1.000 16.217	0.6							9.8631
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	1.6							
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	8	8	9	0.129 2	4	0	3
2.0	0.648 4	0.028 2	22.992 9	- 0.130 4	0.912 9	1.000 0	18.514 6
2.2	0.690 8	0.028 3	24.409 9	- 0.134 0	0.902 7	1.000 0	20.288 1
2.4	0.712 2	0.028 7	24.815 3	- 0.134 0	0.885 4	1.000 0	20.942 1
2.6	0.754 9	0.028 7	26.303 1	0.137 3	0.874 6	1.000 0	22.853 5
2.8	0.776 1	0.029	26.762 1	0.137 0	0.856 5	1.000 0	23.576 5
3.0	0.816 3	0.028 7	28.442 5	- 0.139 1	0.844 9	1.000 0	25.697 6
3.2	0.835 8	0.028 9	28.920 4	- 0.138 1	0.824 7	1.000 0	26.439 7
3.4	0.865 4	0.028 7	30.153 3	0.138 2	0.807 8	1.000 0	28.050 7
3.6	0.896 3	0.028 2	31.783 7	- 0.138 0	0.789 6	1.000 0	30.090 6
3.8	0.918 3	0.028	32.796 4	- 0.136 6	0.767 1	1.000 0	31.428 2
4.0	0.943 1	0.027 6	34.170 3	- 0.135 4	0.745 5	1.000 0	33.183 9
4.2	0.97	0.027 1	35.793 4	0.134 2	0.724 3	1.000 0	35.252 4
4.4	0.994 7	0.026 7	37.254 7	0.132 8	0.700 9	1.000 0	37.155 8
4.6	1.015 4	0.026 5	38.317	- 0.131 1	0.674 4	1.000 0	38.610 9
4.8	1.036 6	0.026 4	39.265 2	- 0.129 4	0.646 3	1.000 0	39.977 2

As shown above, aerodynamic characteristics around the airfoil when the angle of attack varied from 0° to 5° in 0.2° increments at Re = 40000 were analyzed. The optimal angle of attack was 3.4° in the analysis of the loading ratio (Cl / Cd) by comparing the lift coefficient (Cl) and the drag coefficient (Cd). The optimum lift-drag ratio (Cl/Cd) is 30.1533.

3.1.4 MID-103



Fig.7: Two-dimensional cross-section of MID-103 airfoil.

The airfoil MID-103 is characterized to have a maximum thickness of 7.35% at 20.6% of the chord and a maximum camber of 4.50% at 55.0% of the chord.

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Fig. 8: Analysis graph of MID-103 airfoil

Table 4: Analysis results of MID-103 airfoil.

MID	103-Re=4		analysis res		ID-105 all	1011.	
Al-	Cl	Cd	Cl/Cd	Cm	T Xtr	B Xtr	Power
fa 0.0	0.374	0.024	15.273	-	1.000	0.667	F. 9.3431
	2	5	5	0.112 5	0	9	
0.2	0.392		16.144	-	1.000	0.719	10.111
	3	3	0	0.111 9	0	3	6
0.4	0.406	0.024	16.925 0	- 0.110	1.000 0	0.797 4	10.786 9
0.6			-	4			
0.6	0.411 3	0.024	17.066 4	- 0.108 4	1.000 0	1.000 0	10.945 1
0.8	0.435	0.024	17.611	- 0.109	1.000	1.000	11.615 5
	0	/	3	0.109 9	0		5
1.0	0.456	0.025	18.035 6	- 0.110	1.000 0	1.000 0	12.183 0
			-	8		-	
1.2	0.476 2	0.025 9	18.386 1	- 0.111	1.000 0	1.000 0	12.687 7
	0.51.4	0.000		5		1.000	
1.4	0.514 7	0.026	19.422 6	0.115	0.989 6	1.000 0	13.934 3
1.6	0.551	0.026	20.513	5	0.975	1.000	15.237
1.6	0.551	0.026 9	20.513	0.119 1	0.975	1.000	15.237
1.8	0.596 9	0.027	21.784	-	0.963	1.000	16.830
	-		7	0.123	1	0	7
2.0	0.628 7	0.027 8	22.615 1	0.126	0.946 0	1.000 0	17.931 7
2.2	0.674	0.028	24.085	-		1.000	19.779
	4	0	7	0.130 5	8	0	6
2.4	0.701	0.028	24.883	-	0.912	1.000	20.843
	7	2	0	0.131 5	8	0	9
2.6	0.737 4	0.028	26.148 9	0.133	0.895 6	1.000 0	22.454 6
			-	6			
2.8	0.776 4	0.028	27.728 6	0.136	0.878	1.000 0	24.432 6
2.0	0.905	0.029	29.764	0	0.95(1.000	25.014
3.0	0.805 4	0.028	28.764 3	0.136	0.856 4	1.000 0	25.814 2
3.2	0.838	0.027	30.391	-	0.836	1.000	27.834
	8	6	3	0.137 5	3	0	2
3.4	0.876	0.027	32.448	-	0.817	1.000	30.371
	1	0	1	0.138 4	4	0	5
3.6	0.901	0.026	33.883	-	0.791	1.000	32.167
	3	6	5	0.137 6	6	0	9
3.8	0.927	0.026	35.270 0	0.136	0.765 0	1.000 0	33.969 2
	0	5	0	0.130	0	0	2

4.0	0.954	0.025	36.996	-	0.736	1.000	36.144
	5	8	1	0.135	4	0	7
				9			
4.2	0.981	0.025	38.641	-	0.705	1.000	38.282
	5	4	7	0.134	0	0	6
				8			
4.4	1.008	0.025	40.159	-	0.671	1.000	40.319
	0	1	4	0.133	7	0	7
				7			
4.6	1.029	0.025	40.865	-	0.634	1.000	41.469
	8	2	1	0.132	0	0	5
				3			
4.8	1.051	0.025	41.378	-	0.596	1.000	42.420
	0	4	0	0.130	6	0	0
				8			

As shown above, aerodynamic characteristics around the airfoil when the angle of attack varied from 0° to 5° in 0.2° increments at Re = 40000 were analyzed. The optimal angle of attack was 3.4° in the analysis of the loading ratio (Cl / Cd) by comparing the lift coefficient (Cl) and the drag coefficient (Cd). The optimum lift-drag ratio (Cl/Cd) is 32.4481

As a result of aerodynamic analysis, airfoil BE6356 has the largest under camber with 33.6321 of lift-drag ratio (Cl/Cd); however, the lift-drag ratio (Cl/C) of airfoil MID-103 is 32.4484, which has the concept of LDA (low-drag airfoil).

3.2. Glider Selection

According to results of analysis of airfoil, BE6356 with a large under camber and MID-103 with airfoil with LDA (low-drag airfoil) concept were produced as shown in Table 1.

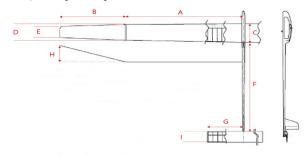


Fig. 9: Glider shape.

Table.5: Glider specifications.								
Specification	Large under camber airfoil glider	LDA concept air- foil glider						
Wing Root Length (A),	680	680						
mm								
Wing Tip Length (B), mm	490	490						
Root Chord (C), mm	150	150						
Dihedral Chord (D),	130	130						
mm								
Tip Chord (E), mm	100	100						
Tail Moment (F), mm	730	730						
Stabilizer Chord (I), mm	85	85						
Stabilizer Length	470	470						
(Gx2), mm								
Wing Tip Height (H),	145	145						
mm								
Dihedral Break, mm	140	140						
Weight, g	412	410.5						
Wing Airfoil	BE6356	MID-103						

3.3. Test Flight

Due to the limitation of the size of $300m \times 800$ m of Osom Airfield in Songsan-myeon, Hwaseong-si, Gyeonggi-do province, Korea at 6 am on May 7, 2018, the glide time was limited to two minutes and two flights were conducted. Two F1A glider national

players flew twice with each model – BE6356 and MID-103. Data were extracted through altimeter built in MTK Timer for flight altitude measurement. Flight data such as speed during bunt maneuver to get off the tow, gain altitude, altitude, and average sink rate during flight are as follows.

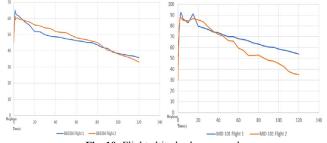


Fig. 10: Flight altitude change graph.

Table. 6: Flight altitude data

	Table. 6: Flight a	altitude data		_	
Flight mode	Time(s)	Altitu	ıde(m)		
Fight mode	Time(s)	Flight 1	Flight 2		Bunt
	0	48.4	45.1		
	0.1	49.5	48.9		
	0.2	50.2	51.3		
	0.3	52.3	51.8		
	0.4	53.4	52.6		
	0.5	57.3	52.6		
	0.6	57.3	54		
	0.7	59.1	56.2		
	0.8	61.2	56.2		
	0.9	63.2	58.9	Bunt	
Bunt	1	63.8	59.5		
	1.1	64.3	60.1		
	1.2	65.2	60.1		
	1.3	65.2	61.2		
	1.4	64.4	61.4		
	1.5	63.8	60.5		
	1.6	63.8	59.1		
	1.7	63.8	59.1		
	1.8	63	59.1		
	1.9	62.7	59.5		
	2	63.2	60.2		
	3	62.1	60.2		
	4	61.9	60.2		
	5	61.3	59.8		
	10	58.2	58.9		
	15	55.8	57.9		
	20	52.1	56.1		
	25	51.8	55.5		
	30	50	54.3		
	35	49.1	53.8		
Glide	40	48.8	52.1		
Glide	45	48.3	51.5		
	50	47.5	51.2	Glide	
	55	47.1	49.7	Gilde	
	60	46.4	48.1	41	
	65	46	47.5		
	70	45.2	46.8	41	
	75	45.1	46	41	
	80	43.8	45.2		
	85	42.1	42.9	41	
	90	41.6	40.2		

	95	39.2	39.8
	100	38.5	38.1
	105	37.8	36.9
	110	37.2	36.1
	115	36.7	34.7
	120	35.9	33.1
Bunt velocity	y(m/s)	7.4	7.6
Vy avg(m	ı/s)	0.23	0.23

		Altitude(m)	
Flight mode	Time(s)	Flight 1	Flight 2
	0	40.6	30
	0.1	48.7	41.3
	0.2	51	44.3
	0.3	54.2	51.7
	0.4	54.2	51.7
	0.5	54.2	51.7
	0.6	65.7	60.6
	0.7	67.8	62.2
	0.8	69.3	64.8
	0.9	70.3	66.8
	1	72.7	68.6
	1.1	78.4	73.4
	1.2	79.2	75.1
	1.3	80.8	76.5
	1.4	81.1	78.3
Bunt	1.5	82.1	79.7
	1.6	83.7	81.9
	1.7	84.9	84.3
	1.8	85.8	84.9
	1.9	86.2	85.1
	2	86.8	85.4
	2.1	88.9	87.9
	2.2	89.8	87.9
	2.3	90.2	87.2
	2.4	90.9	87.4
	2.5	91.5	87.9
	2.6	92	88
	2.7	92	88
	2.8	92	88
	2.9	92	88
	3	92.2	87.7
	4	89.9	86.4
	5	86.6	85.1
	10	82.9	84.6
	15	91.1	86.9
	20	79.8	85.6
	25	78.3	83.9
	30	76.8	78.9
	35	74.5	75
Glide	40	73.7	72.6
	45	71.9	70.4
	50	70.3	66.5
	55	70.1	65.9
	60	68.3	59.6
	65	67.5	57.3
	70	66.1	52.9
	75	64.3	52.7
	-		

	80	63.4	53
	85	61.7	50.3
	90	60.7	48
	95	60.3	47.4
	100	58.8	45.1
	105	57.6	42.6
	110	56.6	38.1
	115	55.3	36.1
	120	54	35.1
Bunt velocity(m/s)		17.2	19.2
Vy avg(m/s)		0.34	0.45

As shown above, the MID-103 airfoil glider rose at an average speed of 18.2m/s during the bunt maneuver and started to glide at 28.25m higher altitude than the BE6356 airfoil glider. However, BE6356 airfoil glider showed lower average sink rate than the MID-103 airfoil glider at 0.17 m/s.

4. Conclusion

F1A glider is a flying body where the performance of the flight endurance is emphasized. To achieve good performance in the regulated range in which the set times are summed and ranked in each round, high altitude acquisition and gliding needs to be ensured when launching before beginning gliding flight. To ensure the gliding property, a wing design with a large aspect ratio and a large camber airfoil should be used for high lift coefficients even at low angle of attack. In this paper, an aerodynamic analysis of a large under camber airfoil BE6356 and airfoil MID-103 with lowdrag airfoil (LDA) was conducted through test flights. As a result, BE6356 airfoil glider can glide at a lower sink rate than MID-103 airfoil glider at 0.17 m/s.

However, at the beginning of the gliding flight, the MID-101airfoil glider started to glide at an average height of 28.25 m. By comparing the altitude at which the glide starts and the sink rate, MID-103airfoil glider is advantageous in F1A glider competition.

5. Discussion

Currently, the history of domestic aviation sports has a starting point from model aircraft. As of 2017, there are more than 100,000 model aircraft competitors in Korea. In recent years, performances of athletes have improved, achieving good results in various world championships. Behind the development of domestic model aircraft market, various intensive technologies of model aircraft play a major role. However, performances of athletes participating in model aircraft competitions have been averaging to a certain extent. Their performances tend to depend on the performance of the model rather than the performance of the athletes. Therefore, it is necessary to develop various models. Model aircraft is a miniature version of a general airplane. It requires very precise technology. This technology is very important for achieving fundamental technology integration of Korea's aviation basic industry in the future. By determining glider performance according to glider airfoil, this study has the following implications.

First, it is possible to determine the optimized lift-to-drag ratio according to angle of attack through airfoil data analysis.

Second, it is possible to determine flight altitude and sink rate.

Third, through data analyses, a more scientific approach is possible when operating the competition.

Fourth, this study provides basic data for the development of domestic aviation industry.

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