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Research paper



# Distribution Generation Optimal Placement with Various Power Factors and Loading Margins

Kalidas Babu Gera<sup>1</sup>, Dr. P.V. Ramana rao<sup>2</sup>

<sup>1</sup> Research scholar, Electrical and Electronics Engineering, A.N.U
 <sup>2</sup> HOD, Electrical and Electronics Engineering, A.N.U
 \*Corresponding author E-mail:kalidas.gera@gmail.com

#### Abstract

In the new era of power system world depleting conventional resources and increasing rapid power demand leads to focus more on distribution power generation or distribution generation (DG). DG contributes to solve numerous issues like to meet out the peak load demand in distribution system, diminishing power system losses and enhance voltage levels. And one of the major issues of distribution generation is to allocate optimally to hold the most benefits. The work in this paper focuses on the optimal placement of DG by considering pre assumed various power factors along with different loading conditions and the study has been carried out by the technique colliding body optimization. This paper also presents a comparison and influence of variations in DG optimal location with pre assumed load power factors 0.85, 0.87, and 0.89 corresponding to the various loading margins of 0.7, 1.0 and 1.25 of total real power load. The above analysis effectively implemented and tabulated for standard 38 bus system in radial distribution network.

Keywords: Colliding bodies' optimization; distributed generation; load margins, radial distribution system.

## 1. Introduction

The primary eminence of power system is to supply unceasing and assurance electricity. This requires continuous power generation from different sources, huge power can be generating through traditional power plants are located hundreds of kilometers distance from load centers. In the present scenario due to rapid growth in electrical utilities the power from traditional generation in not adequate and moreover huge amount of power losses being happening while transmits power for long distances [1]. The other alternative to minimize the burden on traditional power plants, transmission power losses and to maintain voltage in limits a new era was raised called distribution generation (DG). Furthermore many types of DG sources were available for power generation due to their major technical benefits [2] [3] [4] and setting up of alternate energy for electricity has developed at a yearly rate of 25% [5]. Several papers are concentrated on the subject of optimal location and sizing of distributed generators to enhance voltage levels and to reduce power losses [6][7]. This work contributes best possible location of distributed generation for the given bus system by considering the variation in loading margins and pre assumed load power factors in radial distribution networks.

# Objective function = (ILP + ILQ = IVD)(1)

$$ILQ = \left[\frac{\text{total reactive power loss with DG}}{\text{total reactive power loss without DG}}\right](3)$$
$$IVD = Max \left[\frac{|V_s - ||V_i|}{||v_s||}\right]$$
(4)

With Equality constraints,

i=2

$$P_{gs} + \sum_{DG=1}^{m} P_{DG} = P_{demand} + P_{loss}$$
<sup>(5)</sup>

Equality constraints,

$$V_{i\min} \le V_i \le V_{i\max} \tag{6}$$

### 3. Colliding Bodies Optimization

The major intention is to recognize the best possible position of distrib<sup>The</sup> projected method enlarged by kaveh and mahdavi imuted generation and tumbling the impact of power system losses and elled by the normal occurrence of collision involving two voltage profile indices. Now, the main concern is given to renewable<sup>bjective</sup> bodies [8] DGs outstanding of the low maintenance and cost.



2. Mathematical Approach

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#### 3.1. Physical Laws of Collision

Law of collision between two objective bodies is supervised by converse law of momentum and energy. Assume two masses of bodies  $m_1 \& m_2$  travelling in one dimensional space, the momentum of  $m_1 \& m_2$  collision before & after represents in the below figure 1.

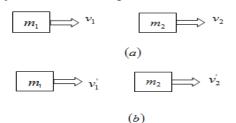


Fig.1: (a) and (b) collision before and after among two bodies.

Constancy of entire force before and after collision is alike directed by subsequent equation

$$m_1 v_1 + m_2 v_2 = m_1 v_1 + m_2 v_2 \tag{7}$$

Besides, the constancy of entire kinetic energy is directed by:

$$\frac{1}{2}m_1v_1^2 + \frac{1}{2}m_2v_2^2 = \frac{1}{2}m_1v_1^2 + \frac{1}{2}m_2v_2^2 + Q$$
(8)

 $v_1$ ,  $v_2$  stand for early velocity of first and second object before contact  $v_1$ ,  $v_2$  represent end velocities of first and second object after contact.  $m_1$ ,  $m_2$  reflects mass of objects, and the Q represents loss of kinetic energy owed in contact [9].

Velocities subsequent to one-dimensional collision,

$$V_{1}' = \frac{(m_{1} - \varepsilon m_{2})v_{1} + (m_{2} + \varepsilon m_{2})v_{2}}{m_{1} + m_{2}}$$
(9)

$$V_{2}' = \frac{(m_{2} - \varepsilon m_{1})v_{2} + (m_{1} + \varepsilon m_{1})v_{1}}{m_{1} + m_{2}}$$
(10)

 $\epsilon$  represent restitution multiplication between the collision of two bodies, defined as ratio of variation in velocity separation to velocity access.

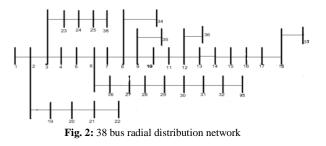
$$\varepsilon = \frac{\left| v_{2}^{'} - v_{1}^{'} \right|}{\left| v_{2} - v_{1} \right|} = \frac{v^{'}}{v}$$
(11)

#### 3.2. Structure of algorithm

In the colliding bodies optimization, each resolution aspirant  $X_i$  comprise several variables  $(i.e \ X_i = \{x_{i,j}\})$  marked as colliding bodies [10]. The colliding bodies optimization algorithm [11] has been taken and implemented.

#### 4. Results

The test data of 38 bus proposed radial distribution network [12] is appearance in figure 2.



12.66 kV is the substation voltage and the total power load is 2.0MW real power and 0.970MVAR with total losses 20.2KW and 13.4847KVAR. The proposed technique for optimal location of DG having size of 1338.55 KVA is carried and implemented on 38 bus radial distribution network.

 Table 1: voltage profiles on different loading factors without DG

| Load margins | 0.75 (P +j Q) | 1.0 (P +j Q) | 1.25 (P + jQ) |
|--------------|---------------|--------------|---------------|
| V1           | 1             | 1            | 1             |
| V2           | 0.9978        | 0.997        | 0.9962        |
| V3           | 0.9874        | 0.9829       | 0.9783        |
| V4           | 0.9819        | 0.9755       | 0.9688        |
| V5           | 0.9765        | 0.9681       | 0.9593        |
| V6           | 0.963         | 0.9497       | 0.9358        |
| V7           | 0.9604        | 0.9462       | 0.9314        |
| V8           | 0.9569        | 0.9414       | 0.9252        |
| V9           | 0.9523        | 0.9351       | 0.9172        |
| V10          | 0.948         | 0.9293       | 0.9098        |
| V11          | 0.9474        | 0.9285       | 0.9087        |
| V12          | 0.9463        | 0.927        | 0.9068        |
| V13          | 0.9448        | 0.9249       | 0.9041        |
| V14          | 0.9431        | 0.9227       | 0.9012        |
| V15          | 0.9421        | 0.9213       | 0.8994        |
| V16          | 0.9411        | 0.9199       | 0.8977        |
| V17          | 0.9396        | 0.9179       | 0.8951        |
| V18          | 0.9392        | 0.9173       | 0.8943        |
| V19          | 0.9974        | 0.9965       | 0.9956        |
| V20          | 0.9963        | 0.995        | 0.9936        |
| V21          | 0.9957        | 0.9943       | 0.9928        |
| V22          | 0.9953        | 0.9936       | 0.992         |
| V23          | 0.9847        | 0.9794       | 0.9738        |
| V24          | 0.9798        | 0.9727       | 0.9654        |
| V25          | 0.9773        | 0.9694       | 0.9612        |
| V26          | 0.9616        | 0.9478       | 0.9334        |
| V27          | 0.9597        | 0.9452       | 0.9301        |
| V28          | 0.9513        | 0.9338       | 0.9154        |
| V29          | 0.9453        | 0.9256       | 0.9049        |
| V30          | 0.9427        | 0.922        | 0.9004        |
| V31          | 0.9396        | 0.9178       | 0.895         |
| V32          | 0.939         | 0.9169       | 0.8939        |
| V33          | 0.9388        | 0.9166       | 0.8935        |
| V34          | 0.9569        | 0.9414       | 0.9252        |
| V35          | 0.9523        | 0.9351       | 0.9172        |
| V36          | 0.9463        | 0.927        | 0.9068        |
| V37          | 0.9392        | 0.9173       | 0.8943        |
| V38          | 0.9773        | 0.9694       | 0.9612        |

 
 Table 2: Losses and voltage sensitivity index on different loading factors without DG

| Load margins | 0.75(P +j Q) | 1.0(P +j Q) | 1.25 (P +j Q) |
|--------------|--------------|-------------|---------------|
| P loss in KW | 107.8694     | 199.1061    | 323.8657      |
| Q loss in KW | 73.2587      | 135.2761    | 220.1387      |
| V index      | 0.0436       | 0.0593      | 0.0757        |

**Table 3:** Voltage profiles on factors 0.75 & 1.0 loading of various power factors with DG

| gins         different power<br>factors         different power<br>factors           PF         0.85         0.87         0.89         0.988         0.998         0.998         0.998         0.998         0.998         0.998         0.998         0.998         0.998         0.998         0.998         0.998         0.998         0.998         0.998         0.989         0.989         0.989         0.989         0.989         0.989         0.989         0.989         0.989         0.989         0.981         0.981         0.981         0.981           V4         0.991         0.991         0.985         0.985         0.985         0.985         0.985         0.981         0.981         0.981           V5         0.9885         0.985         0.985         0.973         0.973         0.973         0.973         0.973         0.973         0.973         0.973         0.973         0.975         0.975         0.955         0.955         0.955         0.955         0.952         0.952         0.952         0.952         0.952         0.952         0.952         0.952         0.952         0.952         0.952         0.952         0.951         0.951         0.951         0.951         0.951 <th>ous power fa</th> <th></th> <th></th> <th>ith</th> <th>1.0</th> <th><math>(\mathbf{D} \downarrow \mathbf{i} \mathbf{O})</math></th> <th>with</th> | ous power fa |       |                    | ith   | 1.0               | $(\mathbf{D} \downarrow \mathbf{i} \mathbf{O})$ | with  |  |
|---|--------------|-------|--------------------|-------|-------------------|---|-------|--|
| PF         0.85         0.87         0.89         0.85         0.87         0.89           VI         1         1         1         1         1         1           V2         0.998         0.998         0.998         0.998         0.998         0.998           V3         0.993         0.991         0.991         0.991         0.991         0.985         0.985           V4         0.991         0.991         0.991         0.981         0.985         0.985           V4         0.991         0.989         0.989         0.981         0.981         0.981           7         7         7         8         9         9           V6         0.985         0.985         0.983         0.981         0.981         0.981           0.985         0.985         0.985         0.985         0.969         0.969           1         1         9         9         8         2         2         1           V7         0.983         0.981         0.965         0.965         0.965         0.965           1         0.977         0.979         0.979         0.951         0.951         0.951 <th>Load mar-</th> <th></th> <th colspan="2">0.75 (P +j Q) with</th> <th colspan="4">1.0 (P +j Q) with</th>   | Load mar-    |       | 0.75 (P +j Q) with |       | 1.0 (P +j Q) with |   |       |  |
| PF         0.85         0.87         0.89         0.85         0.87         0.89           V1         1         1         1         1         1         1         1           V2         0.998         0.998         0.998         0.998         0.998         0.998           V3         0.993         0.993         0.993         0.993         0.989         0.989         0.989           V4         0.991         0.991         0.991         0.985         0.985         0.985         0.981         0.981           V5         0.989         0.989         0.989         0.989         0.989         0.980         0.969           V6         0.985         0.985         0.985         0.973         0.973         0.973           0.970         0.970         0.979         0.979         0.969         0.969         0.969           1         1         9         9         8         2         1         1           V9         0.975         0.975         0.975         0.953         0.953         0.953           2         2         1         1         1         1         1         1         1 <t< th=""><th>gins</th><th colspan="2">-</th><th colspan="3"></th></t<>   | gins         | -     |                    |       |                   |   |       |  |
| V1         1         1         1         1         1         1         1           V2         0.998         0.998         0.998         0.998         0.998         0.998         0.998         0.998         0.998         0.998         0.998         0.998         0.989         0.989         0.989         0.989         0.989         0.989         0.985         0.985         0.985         0.985         0.985         0.981   | DE           | 0.95  |                    | 0.00  | 0.95              |   | 0.90  |  |
| V2         0.998         0.998         0.998         0.998         0.998         0.998         0.998           V3         0.993         0.993         0.993         0.993         0.989         0.989         0.989           V4         0.991         0.991         0.991         0.991         0.991         0.985         0.985         0.985         0.985         0.985         0.981         0.961         0.962         0.962         0.962         0.962         0.952         0.952         0.952         0.952         0.952         0.952         0.952         0.952         0.952         0.952         0.951  |              | -     |                    | 1     | 1                 |   |       |  |
| 7         7         7         7         7         100         1000           V3         0.993         0.993         0.993         0.993         0.989         0.989         0.989         0.989         0.985         0.985         0.985         0.985         0.985         0.985         0.981         0.981         0.981         0.981         0.981         0.981         0.981         0.981         0.981         0.981         0.981         0.981         0.981         0.981         0.983         0.983         0.983         0.983         0.989         0.989         0.983         0.983         0.983         0.969         0.966         0.965         0.965         0.965         0.965         0.965         0.965         0.965         0.965         0.965         0.965         0.952         0.953         0.953         0.953         0.953         0.953         0.953         0.951<  |              |       |                    | -     | -                 |   |       |  |
| 2         2         2         0         0           V4         0.991         0.991         0.985         0.985         0.985         0.985           V5         0.989         0.989         0.989         0.989         0.981         0.981         0.981           V6         0.985         0.985         0.973         0.973         0.973         0.973           6         6         5         3         3         2           V7         0.983         0.983         0.969         0.969         0.969           1         1         9         9         8           V8         0.979         0.979         0.979         0.955         0.959           2         2         1         1         1         1           V10         0.971         0.970         0.952         0.952         0.951           1         0.971         0.970         0.975         0.955         0.951         0.951           V11         0.967         0.967         0.949         0.949         0.949           V13         0.966         0.966         0.945         0.945         0.945           V14         0.965  | V2           |       |                    |       | 0.998             | 0.998   | 0.998 |  |
| V4         0.991         0.991         0.981         0.985         0.985         0.985         0.985         0.985         0.981         0.973         0.973         0.973         0.973         0.973         0.973         0.973         0.975         0.975         0.975         0.975         0.975         0.975         0.975         0.975         0.975         0.975         0.975         0.952         0.954         0.944         0.944         0.   | V3           |       |                    |       | 0.989             | 0.989   | 0.989 |  |
| V5         0.989         0.989         0.981         0.981         0.981         0.981         0.981           V6         0.985         0.985         0.985         0.973         0.973         0.973           V7         0.983         0.983         0.983         0.969         0.969         0.969           1         1         9         9         8         0.969         0.969           V7         0.983         0.979         0.979         0.975         0.969         0.969           V8         0.979         0.975         0.975         0.959         0.959         0.959           2         2         1         1         1         1         1           V10         0.971         0.970         0.970         0.952         0.952         0.952           V11         0.969         0.960         0.960         0.961         0.951         0.951         0.951           V12         0.967         0.967         0.967         0.949         0.948         2           V14         0.966         0.966         0.966         0.945         0.945         0.945           3         2         1         6  | V4           |       |                    |       |                   |   |       |  |
| V6         0.985         0.985         0.985         0.973         0.973         0.973         0.973         0.973         0.973         0.973         0.973         0.973         0.973         0.973         0.973         0.973         0.973         0.973         0.973         0.973         0.979         0.969         0.969         0.969         0.969         0.969         0.969         0.969         0.969         0.965         0.965         0.965         0.965         0.959         0.959         0.959         0.959         0.959         0.959         0.959         0.959         0.959         0.959         0.951         0.951         0.951         0.951         0.951         0.951         0.951         0.951         0.951         0.951         0.951         0.951         0.951         0.951         0.951         0.951         0.951         0.951         0.944         0.949         9         8         2         1 </th <th>V5</th> <th>0.989</th> <th>0.989</th> <th>0.989</th> <th>0.981</th> <th>0.981</th> <th>0.981</th>   | V5           | 0.989 | 0.989              | 0.989 | 0.981             | 0.981   | 0.981 |  |
| V7         0.983         0.983         0.983         0.969         9.969         8.8           V8         0.979         0.979         0.979         0.965         0.965         0.965           V9         0.975         0.975         0.975         0.959         0.959         0.959           2         2         1         1         1         9         5         4         3           V10         0.971         0.970         0.952         0.952         0.952         0.952         0.952           4         4         3         6         6         5         1         9         8         2         1         1         1         9         1         0.951         0.951         0.951         0.951         0.951         0.951         0.951         0.951         0.951         0.951         0.949         9         8         2         1         9         8         2         1         9         8         2         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1  | V6           | 0.985 | 0.985              | 0.985 | 0.973             | 0.973   | 0.973 |  |
| $\begin{array}{c c c c c c c c c c c c c c c c c c c $  | V7           |       |                    |       |                   |   |       |  |
| 765221V90.9750.9750.9750.9750.9590.9590.959221111V100.9710.9710.9700.9520.9520.95300.9700.9700.9700.9520.9520.952443665V120.9690.9690.9690.9510.9510.95143221-V130.9670.9670.9670.9490.94998821V140.9660.9660.9640.9440.944321654V150.9650.9650.9650.9450.945321654V160.9640.9640.9440.9440.94432165V170.9620.9620.9620.9410.9410.941443776V170.9970.9970.9970.9970.9970.99733555V200.9970.9970.9970.9950.9950.9952222666V180.9960.9960.9950.9950.9950.99520.9960.9960.9960.9950.995 <th>\$70</th> <th></th> <th></th> <th>0.070</th> <th>1</th> <th></th> <th></th>  | \$70         |       |                    | 0.070 | 1                 |   |       |  |
| 2         2         1         1         1         1           V10         0.971         0.971         0.970         0.953         0.953         0.953           V11         0.970         0.970         0.970         0.952         0.952         0.952           4         4         3         6         6         5           V12         0.969         0.969         0.969         0.951         0.951         0.951           4         3         2         1         -         -         -           V13         0.967         0.967         0.949         0.949         0.949           9         8         8         2         1         -         -           V14         0.966         0.966         0.964         0.944         0.944         0.944           3         2         1         6         5         4           V15         0.962         0.962         0.942         0.944         0.944         0.944           3         3         2         3         2         1         -           V17         0.962         0.962         0.941         0.941         0.941   |              | 7     | 6                  | 5     | 2                 | 2   | 1     |  |
| Image         9         5         4         3           V11         0.970         0.970         0.970         0.952         0.952         0.952           4         4         3         6         6         5           V12         0.969         0.967         0.967         0.949         0.949         0.949           4         3         2         1         1         1           V13         0.967         0.967         0.949         0.949         0.949           9         8         2         1         1         9         8           V14         0.966         0.966         0.967         0.945         0.945         0.945           3         2         1         6         5         4         4           V16         0.964         0.964         0.944         0.944         0.944         0.944           3         3         2         1         6         5         4           V17         0.962         0.962         0.941         0.941         0.941         0.941           9         8         7         3         3         5         5 <tr< th=""><th></th><th></th><th></th><th></th><th></th><th></th><th></th></tr<>  |              |       |                    |       |                   |   |       |  |
| V11         0.970         0.970         0.970         0.952         0.952         0.952         0.952           V12         0.969         0.969         0.969         0.969         0.951         0.951         0.951           V13         0.967         0.967         0.967         0.967         0.949         0.949         0.949           9         8         2         1         1         1           V14         0.966         0.966         0.967         0.947         0.949         0.949           9         8         2         1         9         8           V14         0.966         0.966         0.967         0.944         0.944         0.944           3         2         1         9         8           V15         0.964         0.964         0.964         0.964         0.944         0.944           3         2         0.962         0.962         0.962         0.942         0.942         0.942           9         8         7         3         3         2         1           V17         0.962         0.962         0.962         0.941         0.941         0.941   | V10          | 0.971 | 0.971              |       |                   |   |       |  |
| V12         0.969         0.969         0.969         0.951         0.951         0.951           V13         0.967         0.967         0.967         0.949         0.949         0.949           9         8         2         1         -         -           V14         0.966         0.966         0.965         0.947         0.949         0.949           3         2         1         9         8           V15         0.965         0.965         0.945         0.945         0.945           3         2         1         6         5         4           V16         0.964         0.964         0.944         0.944         0.944           3         2         3         2         1           V16         0.962         0.962         0.942         0.942         0.942           9         8         7         3         3         2         1           V17         0.962         0.962         0.941         0.941         0.941           4         4         3         7         7         6           V19         0.998         0.997         0.997   | V11          |       |                    | 0.970 | 0.952             | 0.952   | 0.952 |  |
| V13         0.967         0.967         0.967         0.949         0.949         0.949           V14         0.966         0.966         0.966         0.947         0.946         0.946           3         2         1         9         8           V15         0.965         0.965         0.945         0.945         0.945           3         2         1         6         5         4           V16         0.964         0.964         0.944         0.942         0.942           3         2         3         2         1         6         5           V16         0.964         0.964         0.964         0.944         0.942         0.942           9         8         7         3         2         1           V17         0.962         0.962         0.962         0.942         0.942         0.942           9         8         7         3         3         2         0.941         0.941         0.941           4         4         3         7         7         6         9         9         9         9           V20         0.997         0.997   | V12          | 0.969 | 0.969              | 0.969 | 0.951             | 0.951   |       |  |
| V14         0.966         0.966         0.966         0.947         0.946         0.946           3         2         1         9         8           V15         0.965         0.965         0.965         0.945         0.945         0.945           3         2         1         6         5         4           V16         0.964         0.964         0.964         0.944         0.944         0.944           3         3         2         3         2         1           V17         0.962         0.962         0.962         0.942         0.942         0.942           9         8         7         3         3         2         0.942           V18         0.962         0.962         0.962         0.941         0.941         0.941           4         4         3         7         7         6           V19         0.998         0.998         0.997         0.997         0.997         0.997           2         2         2         9         9         9           V21         0.996         0.996         0.996         0.9975         0.9975         0.9978  | V13          | 0.967 | 0.967              | 0.967 | 0.949             | 0.949   | 0.949 |  |
| V15         0.965         0.965         0.965         0.945         0.945         0.945           3         2         1         6         5         4           V16         0.964         0.964         0.964         0.944         0.944         0.944           3         2         3         2         1           V17         0.962         0.962         0.962         0.942         0.942         0.942           9         8         7         3         3         2           V18         0.962         0.962         0.962         0.941         0.941         0.941           4         4         3         7         6         7         7           V19         0.998         0.998         0.997         0.997         0.997         0.995         0.995         0.995           2         2         2         9         9         9         9           V20         0.997         0.997         0.997         0.995         0.995         0.995         0.995           2         2         2         2         6         6         6         9         7           V21   | V14          | 0.966 | 0.966              | 0.966 |                   | 0.946   |       |  |
| V16         0.964         0.964         0.964         0.944         0.944         0.944           3         3         2         3         2         1           V17         0.962         0.962         0.962         0.942         0.942         0.942           9         8         7         3         3         2           V18         0.962         0.962         0.962         0.941         0.941         0.941           4         4         3         7         7         6           V19         0.998         0.998         0.997         0.997         0.997         0.997           3         3         5         5         5         5           V20         0.997         0.997         0.997         0.995         0.995         0.995           2         2         9         9         9         9         9           V21         0.996         0.996         0.996         0.995         0.995         0.995           2         2         2         2         2         2         2         2         2         2         2         2         2         2         2 <th>V15</th> <th>0.965</th> <th>0.965</th> <th></th> <th>0.945</th> <th>0.945</th> <th></th>  | V15          | 0.965 | 0.965              |       | 0.945             | 0.945   |       |  |
| 3         3         2         3         2         1           V17         0.962         0.962         0.962         0.942         0.942         0.942           9         8         7         3         3         2           V18         0.962         0.962         0.962         0.941         0.941         0.941           4         4         3         7         7         6           V19         0.998         0.998         0.997         0.997         0.997           3         3         5         5         5           V20         0.997         0.997         0.997         0.995         0.995           2         2         9         9         9         9           V21         0.996         0.996         0.996         0.995         0.995         0.995           2         2         2         9         9         9         9           V21         0.996         0.996         0.996         0.994         0.994         0.994           2         2         2         6         6         6         6           V23         0.990         0.990 </th <td>V16</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>   | V16          |       |                    |       |                   |   |       |  |
| 9         8         7         3         3         2           V18         0.962         0.962         0.962         0.941         0.941         0.941         0.941           4         4         3         7         7         6           V19         0.998         0.998         0.997         0.997         0.997         0.997           3         3         5         5         5           V20         0.997         0.997         0.997         0.995         0.995         0.995           2         2         2         9         9         9         9           V21         0.996         0.996         0.996         0.996         0.996         0.996         0.996         0.996         0.996         0.995         0.995         0.995           2         2         2         6         7         8         8         8         7         5         5         5   |              | 3     | 3                  | 2     | 3                 | 2   | 1     |  |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$   | V17          |       |                    |       |                   |   |       |  |
| 333555V20 $0.997$ $0.997$ $0.997$ $0.995$ $0.995$ $0.995$ $0.995$ 222999V21 $0.996$ $0.996$ $0.996$ $0.995$ $0.995$ $0.995$ 77222V22 $0.996$ $0.996$ $0.996$ $0.994$ $0.994$ 222666V23 $0.990$ $0.990$ $0.990$ $0.985$ $0.985$ 66645V24 $0.985$ $0.985$ $0.985$ $0.978$ 66788V25 $0.983$ $0.983$ $0.983$ $0.975$ $0.975$ 22255V26 $0.986$ $0.986$ $0.973$ $0.973$ $0.973$ 221443V27 $0.987$ $0.987$ $0.987$ $0.973$ $0.973$ 1776V28 $0.990$ $0.990$ $0.993$ $0.974$ $0.974$ 875864V29 $0.993$ $0.993$ $0.993$ $0.977$ $0.977$ 97485V30 $0.996$ $0.996$ $0.995$ $0.977$ $0.977$ 2 $0.996$ $0.996$ $0.995$ $0.977$ $0.977$  | V18          |       |                    |       |                   |   |       |  |
| $ \begin{array}{c ccccccccccccccccccccccccccccccccccc$  | V19          |       |                    |       |                   |   |       |  |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$   | V20          | 0.997 | 0.997              | 0.997 | 0.995             | 0.995   | 0.995 |  |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$   | V21          | 0.996 | 0.996              | 0.996 | 0.995             | 0.995   | 0.995 |  |
| V23         0.990         0.990         0.990         0.990         0.985         0.985         0.985         0.985         0.985         5           V24         0.985         0.985         0.985         0.985         0.978         0.978         0.978         0.978         0.978           6         6         7         8         8         8           V25         0.983         0.983         0.983         0.975         0.975         0.975           2         2         2         5         5         5           V26         0.986         0.986         0.986         0.986         0.973         0.973         0.973           2         2         1         4         4         3           V27         0.987         0.987         0.987         0.973         0.973         0.973           1         7         7         6           V28         0.990         0.990         0.990         0.974         6           8         7         5         8         6         4           V29         0.993         0.993         0.993         0.975         0.975         0.975           <   | V22          | 0.996 | 0.996              | 0.996 | 0.994             | 0.994   | 0.994 |  |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$   | V23          | 0.990 | 0.990              | 0.990 | 0.985             | 0.985   | 0.985 |  |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$   | V24          |       |                    |       |                   |   |       |  |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$   | V25          |       |                    |       |                   |   |       |  |
| 2         2         1         4         4         3           V27         0.987         0.987         0.987         0.973         0.973         0.973         0.973           1         7         7         6           V28         0.990         0.990         0.990         0.974         0.974         0.974           8         7         5         8         6         4           V29         0.993         0.993         0.993         0.976         0.975         0.975           9         7         4         8         5           V30         0.996         0.996         0.995         0.977         0.977         0.977           2         7         5         3          1         <  |              | 2     | 2                  | 2     | 5                 | 5   | 5     |  |
| 1         7         7         6           V28         0.990         0.990         0.990         0.974         0.974         0.974           8         7         5         8         6         4           V29         0.993         0.993         0.993         0.976         0.975         0.975           9         7         4         8         5           V30         0.996         0.996         0.995         0.977         0.977           2         7         5         3         2   |              | 2     | 2                  | 1     | 4                 | 4   | 3     |  |
| 8         7         5         8         6         4           V29         0.993         0.993         0.993         0.976         0.975         0.975           9         7         4         8         5           V30         0.996         0.996         0.995         0.977         0.977           2         7         5         3         3   |              | 1     |                    |       | 7                 | 7   | 6     |  |
| 9         7         4         8         5           V30         0.996         0.996         0.995         0.977         0.977         0.977           2         7         5         3         3   |              | 8     | 7                  | 5     | 8                 | 6   | 4     |  |
| V30         0.996         0.996         0.995         0.977         0.977         0.977           2         7         5         3         3   | V29          |       |                    |       | 0.976             |   |       |  |
|   | V30          | 0.996 | 0.996              |       |                   | 0.977   |       |  |
|   | V31          | 0.993 | 0.993              | 0.992 | 0.973             | 0.973   | 0.973 |  |

|     | 3     | 1     | 9     | 6     | 4     | 1     |
|-----|-------|-------|-------|-------|-------|-------|
| V32 | 0.992 | 0.992 | 0.992 | 0.972 | 0.972 | 0.972 |
|     | 7     | 5     | 2     | 7     | 5     | 2     |
| V33 | 0.992 | 0.992 | 0.992 | 0.972 | 0.972 | 0.972 |
|     | 5     | 3     |       | 5     | 3     |       |
| V34 | 0.979 | 0.979 | 0.979 | 0.965 | 0.965 | 0.965 |
|     | 7     | 6     | 5     | 2     | 2     | 1     |
| V35 | 0.975 | 0.975 | 0.975 | 0.959 | 0.959 | 0.959 |
|     | 2     | 2     | 1     | 1     | 1     |       |
| V36 | 0.969 | 0.969 | 0.969 | 0.951 | 0.951 | 0.951 |
|     | 4     | 3     | 2     | 2     | 1     |       |
| V37 | 0.962 | 0.962 | 0.962 | 0.941 | 0.941 | 0.941 |
|     | 4     | 4     | 3     | 7     | 7     | 6     |
| V38 | 0.983 | 0.983 | 0.983 | 0.975 | 0.975 | 0.975 |
|     | 2     | 2     | 2     | 5     | 5     | 5     |

 Table 4: Voltage profiles on factor 1.25 loading of various power factors with DG

| Load margins | rs with DG<br>ns 1.25 (P +j Q) with different power factors |        |        |  |  |  |
|--------------|---|--------|--------|--|--|--|
| Power Factor | 0.85  | 0.87   | 0.89   |  |  |  |
| V1           | 1   | 1      | 1      |  |  |  |
| V2           | 0.9972  | 0.9972 | 0.9972 |  |  |  |
| V3           | 0.9847  | 0.9847 | 0.9847 |  |  |  |
| V4           | 0.9791  | 0.9791 | 0.9791 |  |  |  |
| V5           | 0.9737  | 0.9737 | 0.9737 |  |  |  |
| V6           | 0.9605  | 0.9605 | 0.9604 |  |  |  |
| V7           | 0.9562  | 0.9561 | 0.956  |  |  |  |
| V8           | 0.9502  | 0.9501 | 0.95   |  |  |  |
| V9           | 0.9424  | 0.9424 | 0.9422 |  |  |  |
| V10          | 0.9352  | 0.9351 | 0.935  |  |  |  |
| V11          | 0.9341  | 0.9341 | 0.934  |  |  |  |
| V12          | 0.9323  | 0.9322 | 0.9321 |  |  |  |
| V13          | 0.9297  | 0.9296 | 0.9295 |  |  |  |
| V14          | 0.9269  | 0.9268 | 0.9267 |  |  |  |
| V15          | 0.9251  | 0.9251 | 0.925  |  |  |  |
| V16          | 0.9234  | 0.9234 | 0.9233 |  |  |  |
| V17          | 0.9209  | 0.9209 | 0.9208 |  |  |  |
| V18          | 0.9202  | 0.9201 | 0.92   |  |  |  |
| V19          | 0.9966  | 0.9966 | 0.9966 |  |  |  |
| V20          | 0.9946  | 0.9946 | 0.9946 |  |  |  |
| V21          | 0.9938  | 0.9938 | 0.9938 |  |  |  |
| V22          | 0.993   | 0.993  | 0.993  |  |  |  |
| V23          | 0.9802  | 0.9802 | 0.9802 |  |  |  |
| V24          | 0.9718  | 0.9718 | 0.9718 |  |  |  |
| V25          | 0.9677  | 0.9677 | 0.9677 |  |  |  |
| V26          | 0.9602  | 0.9601 | 0.96   |  |  |  |
| V27          | 0.9598  | 0.9598 | 0.9597 |  |  |  |
| V28          | 0.9582  | 0.958  | 0.9578 |  |  |  |
| V29          | 0.9575  | 0.9572 | 0.9569 |  |  |  |
| V30          | 0.9581  | 0.9579 | 0.9576 |  |  |  |
| V31          | 0.9531  | 0.9529 | 0.9526 |  |  |  |
| V32          | 0.952   | 0.9518 | 0.9515 |  |  |  |
| V33          | 0.9517  | 0.9515 | 0.9511 |  |  |  |
| V34          | 0.9502  | 0.9501 | 0.95   |  |  |  |
| V35          | 0.9424  | 0.9424 | 0.9422 |  |  |  |
| V36          | 0.9323  | 0.9322 | 0.9321 |  |  |  |
| V37          | 0.9202  | 0.9201 | 0.92   |  |  |  |
| V38          | 0.9677  | 0.9677 | 0.9677 |  |  |  |

 Table 5: Losses and voltage sensitivity index on .075 load factor with DG

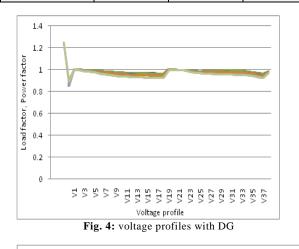
| Load margins   | 0.75 (P + j Q) with different power factors |         |         |  |  |  |
|----------------|---|---------|---------|--|--|--|
| Power factor   | 0.85  | 0.87    | 0.89    |  |  |  |
| PLOSS          | 35.5452                                     | 36.313  | 37.355  |  |  |  |
| QLOSS          | 27.0416                                     | 27.5956 | 28.3356 |  |  |  |
| VINDEX         | 0.021                                       | 0.021   | 0.0211  |  |  |  |
| ILP            | 0.1785                                      | 0.1824  | 0.1876  |  |  |  |
| ILQ            | 0.1999                                      | 0.204   | 0.2095  |  |  |  |
| Location of DG | 30  | 30      | 30      |  |  |  |
|                |   |         |         |  |  |  |

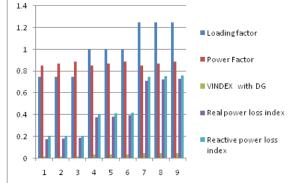
Table 6: Losses and voltage sensitivity index on 1.0 load factor with DG

| Load margins   | 1.0 $(P + j Q)$ with different power factors |         |         |  |  |  |
|----------------|--|---------|---------|--|--|--|
| Power factor   | 0.85   | 0.87    | 0.89    |  |  |  |
| PLOSS          | 75.6364                                      | 76.7209 | 78.1886 |  |  |  |
| QLOSS          | 54.8898                                      | 55.6703 | 56.7105 |  |  |  |
| VINDEX         | 0.0348                                       | 0.0349  | 0.035   |  |  |  |
| ILP            | 0.3799                                       | 0.3853  | 0.3927  |  |  |  |
| ILQ            | 0.4058                                       | 0.4115  | 0.4192  |  |  |  |
| Location of DG | 30   | 30      | 30      |  |  |  |
|                |  |         |         |  |  |  |

Table 7: Losses and voltage sensitivity index on1.25 load factor with DG

| Load margins   | 1.25 ( $P + j Q$ ) with different power factors |          |          |  |  |  |
|----------------|---|----------|----------|--|--|--|
| Power factor   | 0.85  | 0.87     | 0.89     |  |  |  |
| PLOSS          | 142.3226  | 143.7682 | 145.7198 |  |  |  |
| QLOSS          | 100.8835  | 101.9209 | 103.3012 |  |  |  |
| VINDEX         | 0.0496  | 0.0497   | 0.0498   |  |  |  |
| ILP            | 0.7148  | 0.7221   | 0.7319   |  |  |  |
| ILQ            | 0.7458  | 0.7534   | 0.7636   |  |  |  |
| Location of DG | 30  | 30       | 30       |  |  |  |
|                |   |          |          |  |  |  |





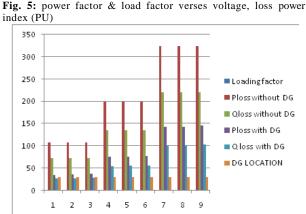


Fig. 6: Total power losses with and without DG for different load margins

| Table 8: 38-bus system data |    |     |         |                              |          |                          |      |       |
|-----------------------------|----|-----|---------|------------------------------|----------|--------------------------|------|-------|
| Bus                         |    |     | Imped   | Line<br>Impedances<br>in p.u |          | Loads on<br>to-bus (p.u) |      |       |
| From                        | То |     | R (p.u) |                              | X (p.u)  | Р                        |      | Q     |
| 1                           | 2  |     | 0.0005  | 74                           | 0.000293 | 0                        | 1    | 0.06  |
| 2                           | 3  |     | 0.00030 |                              | 0.001564 |                          | .09  | 0.00  |
| 3                           | 4  |     | 0.0030  |                              | 0.001304 |                          | .12  | 0.04  |
| 4                           | 5  |     | 0.0022  |                              | 0.001101 |                          | .06  | 0.00  |
| 5                           | 6  |     | 0.0051  | 15                           | 0.004402 |                          | .06  | 0.06  |
| 6                           | 7  |     | 0.0011  | 66                           | 0.003853 | 0                        |      | 0.00  |
| 7                           | 8  |     | 0.0044  |                              | 0.001464 | 0                        |      | 0.1   |
| 8                           | 9  |     | 0.0064  |                              | 0.004608 |                          | .06  | 0.06  |
| 9                           | 10 |     | 0.0065  |                              | 0.004608 |                          | .06  | 0.06  |
| 10                          | 11 |     | 0.0012  |                              | 0.000405 | 0                        | .45  | 0.03  |
| 11                          | 12 |     | 0.0023  |                              | 0.000771 |                          | .06  | 0.035 |
| 12                          | 13 |     | 0.0091  |                              | 0.007192 |                          | .06  | 0.035 |
| 13                          | 14 |     | 0.0033  | 72                           | 0.004439 | 0                        | .12  | 0.08  |
| 14                          | 15 |     | 0.0036  | 8                            | 0.003275 | 0                        | .6   | 0.01  |
| 15                          | 16 |     | 0.0046  | 47                           | 0.003394 | 0                        | .06  | 0.02  |
| 16                          | 17 |     | 0.0080  | 26                           | 0.010716 | 0                        | .06  | 0.02  |
| 17                          | 18 |     | 0.0045  | 58                           | 0.003574 | 0                        | .09  | 0.04  |
| 2                           | 19 |     | 0.0010  | 21                           | 0.000974 | 0                        | .09  | 0.04  |
| 19                          | 20 |     | 0.0093  | 66                           | 0.00844  | 0                        | .09  | 0.04  |
| 20                          | 21 | 0.0 | 0255    | 0.00                         | 2979     |                          | 0.09 | 0.04  |
| 21                          | 22 | 0.0 | 004414  | 0.00                         | 5836     |                          | 0.09 | 0.04  |
| 3                           | 23 | 0.0 | )02809  | 0.00                         | 192      |                          | 0.09 | 0.05  |
| 23                          | 24 | 0.0 | 05592   | 0.00                         | 4415     |                          | 0.42 | 0.2   |
| 24                          | 25 | 0.0 | )05579  | 0.00                         | 4366     |                          | 0.42 | 0.2   |
| 6                           | 26 | 0.0 | 001264  | 0.00                         | 0644     |                          | 0.06 | 0.025 |
| 26                          | 27 | 0.0 | 00177   | 0.00                         | 0901     |                          | 0.06 | 0.25  |
| 27                          | 28 | 0.0 | )06594  | 0.00                         | 5814     |                          | 0.06 | 0.02  |
| 28                          | 29 |     | 05007   |                              | 4362     |                          | 0.12 | 0.07  |
| 29                          | 30 |     | 00316   | 0.00                         |          |                          | 0.2  | 0.6   |
| 30                          | 31 |     | )06067  |                              | 0.005996 |                          | 0.15 | 0.07  |
| 31                          | 32 |     | 01933   | 0.002253                     |          |                          | 0.21 | 0.1   |
| 32                          | 33 |     | 002123  |                              | 0.003301 |                          | 0.06 | 0.04  |
| 8                           | 34 |     | )12453  |                              | 2453     |                          | 0    | 0     |
| 9                           | 35 |     | )12453  |                              | 2453     |                          | 0    | 0     |
| 12                          | 36 |     | )12453  |                              | 2453     |                          | 0    | 0     |
| 18                          | 37 |     | 003113  |                              | 3113     |                          | 0    | 0     |
| 25                          | 38 | 0.0 | 003113  | 0.00                         | 3113     |                          | 0    | 0     |
|                             |    |     |         |                              |          |                          |      |       |

# 5. Conclusion:

A new effort has been made to expansively examine and compare the performance of the DG at different loading factors corresponding to various load power factors has been done by the technique colliding body optimization. This paper elaborately shows comparison and influence of variations in voltage profile and total losses in the system with pre assumed load power factors 0.85, 0.87, and 0.89 corresponding to the various load factors of 0.75, 1 and 1.25 of total real power load. The best possible location of photovoltaic distribution generation is found at bus location at 30<sup>th</sup> bus for all the conditions, hence this method placement of the DG in radial distribution networks have the strong influence on the total power system loss and enhancing desirable voltage levels on the system. The consequences of projected approach have been carried out on standard 38 bus radial distribution network.

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