



# Effect of Grain Modification on Electrical Transport Properties and Electroresistance Behavior of $\text{Sm}_{0.55}\text{Sr}_{0.45}\text{MnO}_3$

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## Abstract

The structural, magnetic, electrical and electroresistance properties of  $\text{Sm}_{0.55}\text{Sr}_{0.45}\text{MnO}_3$  manganites sintered at different sintering temperature of 1300°C (S1) and 1400°C (S2) had been investigated for further potential application as a nonvolatile memory elements. The samples were prepared by using conventional solid-state reaction method. An analysis of x-ray diffraction data using Rietveld analysis show that the sample crystallized in orthorhombic structure and formed pure phase. AC susceptibility measurements showed that the magnetic transition temperature remained unchanged as sintering temperature increased indicated heat treatment process does not much influence the magnetic properties of the samples. Resistivity – temperature curve with different applied currents of 1 mA and 10 mA showed metal-insulator, MI transition temperature,  $T_{MI}$  decreased with increased of the applied currents for sample S1. However, the transition temperature remained unchanged for sample S2. The increased in applied current caused the maximum resistivity around  $T_{MI}$  to be decreased for both samples indicated increased in charge carrier density which resulting in drop of resistivity, hence, enhanced double exchange mechanism. Sample S2 exhibited enhanced in ER effect in the vicinity of M-I transition temperature,  $T_{MI}$  compared to S1 sample which may relate to reduction in scattering effect as a result of reduction of grain boundary density. The observation of ER maximum behavior indicated that the materials are suitable for further investigation as a potential device for spintronic applications.

**Keywords:** Conduction Mechanism; Electroresistance; Grain Modification; Manganites

## 1. Introduction

The observation of electroresistance (ER), was reported in some manganites such as in  $\text{La}_{0.67}\text{Ba}_{0.33}\text{MnO}_3$  [1],  $\text{Nd}_{0.7}\text{Sr}_{0.3}\text{MnO}_3$  [2] and  $\text{PrMnO}_3$  [3], which attributed to the changes in resistance as a results of variation of applied current/voltage [1-3]. The finding of ER effect in such manganites triggered the growth in research/study in manganites due to its potential for practical applications such as nonvolatile memory elements [1-3] and others spintronics based applications such as for communication technologies, magnetic data storage and microelectronics [4]. As reported by Mohan et al. [5],  $\text{Sm}_{0.55}\text{Sr}_{0.45}\text{MnO}$  exhibited metal – insulator (MI) transition with metal-insulator transition temperature,  $T_{MI}$  of 125K under applied current of 1 mA. Interestingly,  $\text{Sm}_{0.55}\text{Sr}_{0.45}\text{MnO}_3$  compound was also reported exhibited ER maximum behavior around  $T_{MI}$ . The Sm-based manganite such as  $\text{Sm}_{0.55}\text{Sr}_{0.45}\text{MnO}_3$  is quite interesting compound due to presence of phase separation which was reported influence the ER effect [5, 6]. The possible mechanism for the observed ER behavior was suggested due to the improved of ordering of localized spins and the other is related to the induced of growth of ferromagnetic regions at low temperature region above  $T_{MI}$  [5]. The intensity of resistivity peak around  $T_{MI}$  of  $\text{Sm}_{0.55}\text{Sr}_{0.45}\text{MnO}_3$  compound reduced when the current was increased from 2.5 mA until 50 mA. On the other hand,  $T_{MI}$  remains unchanged with increasing the electric current while insulating region near to  $T_{MI}$  drop significantly. On the other hand, another report shown that the ER effect was due to presence of inhomogeneities which related to the presence of mixed phase such as in  $\text{Sm}_{0.60}\text{Sr}_{0.40}\text{Mn}_{1-x}\text{FexO}_3$  compound [7]. This suggest that mechanism behind the observation of drop

of resistivity as well as the existence of ER especially in Sm-based compounds could be due to other factors which need further investigation. It was also reported that the ER behavior was strongly influenced by the microstructure of the materials, such as in  $\text{Nd}_{0.7}\text{Sr}_{0.3}\text{MnO}_3$  [2]. Interestingly, the modification of microstructure was also found affect the formation of inhomogeneity as well as the electrical and magnetic properties such as in  $\text{La}_{0.8}\text{Ca}_{0.3}\text{MnO}_3$  compound [8]. Therefore the grain modification is also expected to have an effect on ER behavior, however, there were no details reports on how grain modification can affect the behavior of colossal ER in  $\text{Sm}_{0.55}\text{Sr}_{0.45}\text{MnO}_3$ . In addition to that, the microstructures of ceramic materials are strongly influenced by preparation techniques such as variation of sintering temperature [2]. Therefore, the different of sintering temperature,  $T_S$  were applied in preparation of  $\text{Sm}_{0.55}\text{Sr}_{0.45}\text{MnO}_3$  compound during heat treatment process in order to investigate the effect of grain modification on ER effect behavior. The study of this  $\text{Sm}_{0.55}\text{Sr}_{0.45}\text{MnO}_3$  is expected to give more explanations and knowledge about the possible mechanism involved for the observed ER behavior of the compound. Besides that, the effect of microstructure and different applied current on transport behavior was further investigated by analysis the experimental resistivity data based on scattering and hopping models both in metallic and insulating region to understand the nature of the ER behavior.

## 2. Methodology

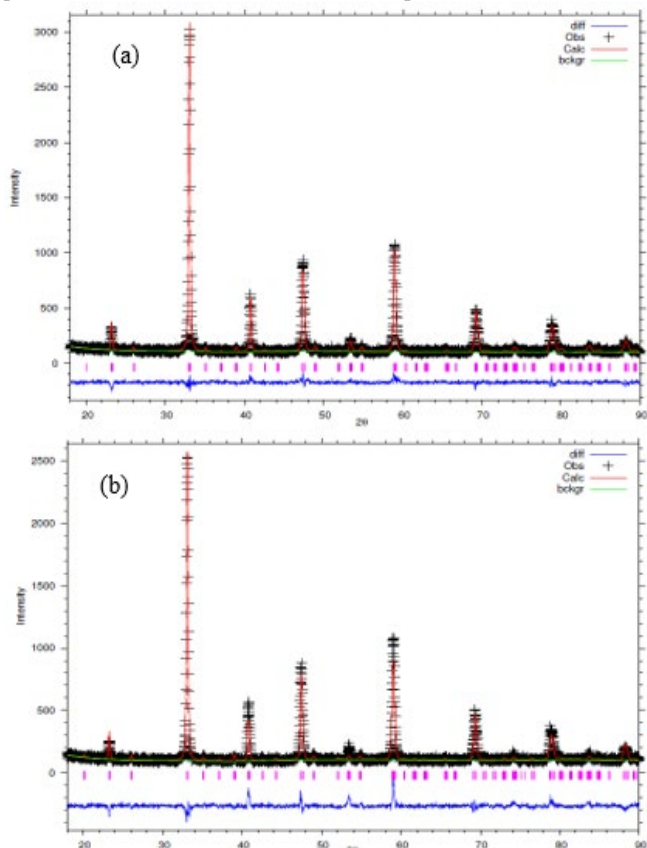
$\text{Sm}_{0.55}\text{Sr}_{0.45}\text{MnO}_3$  was synthesized by the conversational solid-state synthesis method. During the preparation, stoichiometric amounts of  $\text{Sm}_2\text{O}_3$ ,  $\text{SrCO}_3$ , and  $\text{MnO}_2$  oxides powder with high

purity (>99.99 %) were mixed, ground and then calcined at 950 °C for 24 hours with one intermediate grinding. After the final grinding, the powder obtained was pressed into pellet and sintered at 1300 °C (sample S1) and 1400 °C (sample S2), respectively for 24 hours. The structural characterization of the samples was done using X-ray diffraction (XRD) technique using a PANalytical model Xpert PRO MPD diffractometer with CuK $\alpha$  radiation to determine their crystal structure and phase. The electrical and electroresistance (ER) behaviors were carried out using the standard four-point probe technique as a function of temperature (18-300 K) in a Janis model CCS 350ST cryostat under applied current of 1 mA and 10 mA, respectively. AC susceptibility measurements were carried out with variation of temperature down to 20 K and the real components were resolved using a Signal Recovery 7265 lock-in amplifier.

### 3. Results and Discussions

#### 3.1. Structural Analysis

Fig. 1 shows the measured XRD diffraction pattern at room temperature with the refined diffraction pattern for Sm<sub>0.55</sub>Sr<sub>0.45</sub>MnO<sub>3</sub> sintered at different temperatures. The position of the diffraction peaks for both S1 and S2 samples are found similar as reported by Mohan et al. [5], Giri et al. [6] and Abramovich et al. [8]. There are no present of impurities as a result of variation in sintering temperatures. In this case, it can be said that the phase formation for the samples are not influenced by the change of sintering temperature. An analysis of diffraction data by using Rietveld refinement showed that the samples can be categorized as single-phase orthorhombic structure with lattice parameter  $a \neq b \neq c$ .



**Fig. 1:** Refined XRD pattern of Sm<sub>0.55</sub>Sr<sub>0.45</sub>MnO<sub>3</sub> (S1 and S2). The measured diffraction pattern (black curve) is shown together with the refined diffraction pattern (red curve) and their difference pattern (blue line below).

Table 1 shows the calculated lattice parameters and the unit cell volume for both samples. The obtained calculated lattice parameters for S1 (1300°C) and S2 (1400°C) is similar as reported in

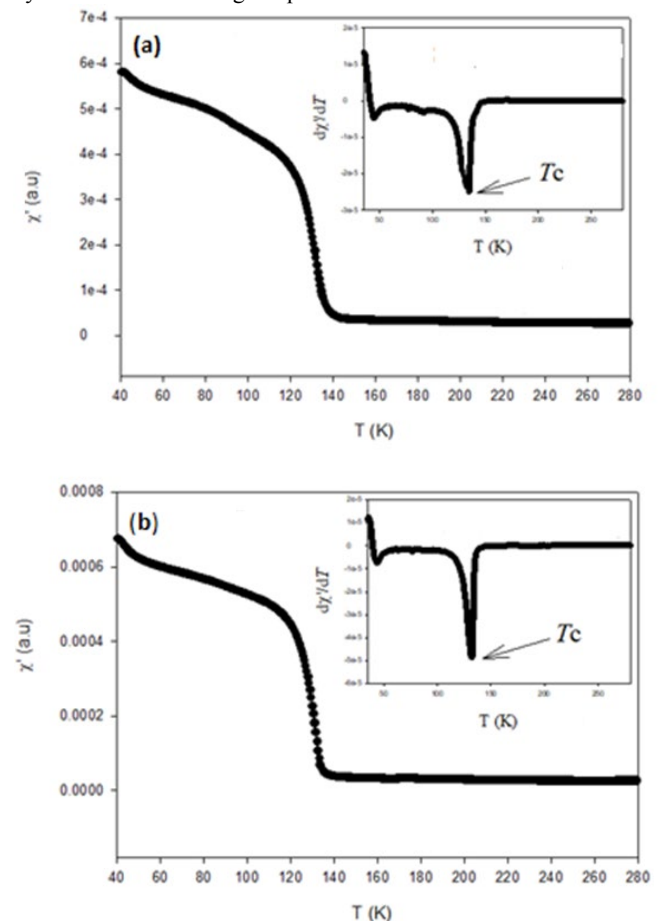
previous report by Abramovich et al. [9] and Mohan et al. [5]. It was found that unit cell volume slightly decreased as sintering temperature increased. The value of  $\chi^2$  obtained is in the acceptable range which is 1.061 and 1.467 for sample S1 and S2, which reflect the high quality of fitting between experimental data and the theoretical data.

**Table 1:** Lattice parameters and unit cell volume of samples: Sm<sub>0.55</sub>Sr<sub>0.45</sub>MnO<sub>3</sub> (S1 and S2)

Sampl	a (Å)	b(Å)	c(Å)	Unit Cell Volume(Å <sup>3</sup> )	$\chi^2$
S1	5.4313(6)	7.6611(5)	5.4407(7)	226.39(6)	1.061
S2	5.4401(9)	7.6617(7)	5.4288(6)	226.27(7)	1.467

#### 3.2. Magnetic Properties

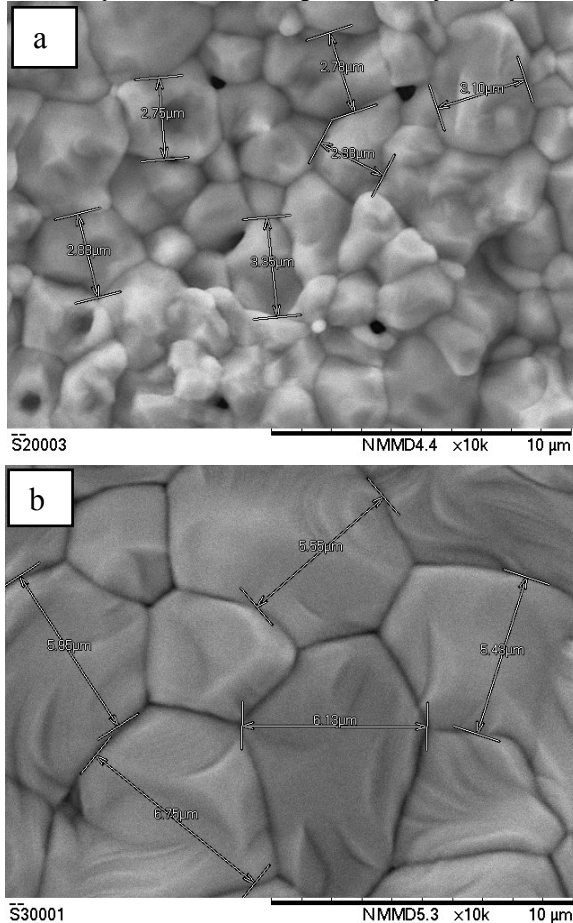
Fig. 2a and 2b show the in-phase susceptibility component,  $\chi'$  versus temperature for both samples S1 and S2. All samples exhibited ferromagnetic (FM) to paramagnetic (PM) transitions. For sample S1, ferromagnetic-paramagnetic transition temperature,  $T_c$  is observed at 134.7K as shown in the inset of Fig. 2a and 2b, while for sample S2 the  $T_c$  is at 132.2K. It is found that transition temperature slightly decreased but not much change with increased in sintering temperature, indicating the magnetic phase transition took place nearly at the same temperature. As reported by Yang et al. [10], the  $T_c$  of sample La<sub>0.9</sub>Te<sub>0.1</sub>MnO<sub>3</sub> was observed to be slightly decreased but not much change with increasing the grain size, which suggested  $T_c$  value not much influenced by variation of sintering temperature.



**Fig. 2:** Temperature dependence of real ( $\chi'$ ) parts for both samples S1 (a) and S2 (b). Inset shows the Curie temperature,  $T_c$ , determined from the minima of  $d\chi'/dT$  versus T curve.

The observed broad FM region indicated increased in sintering temperature influenced the growth of FM phase at low temperature region. As sintering temperature increased, the grain sizes increased as shown in Fig. 3a and 3b. For sample S1, the scanning

electron microscope (SEM) image clearly showed well formation of grain with grain size is around  $2.87\mu\text{m}$ . Further, increase of sintering temperature to  $1400^\circ\text{C}$  enlarged the grain size and improved connectivity between grains. The estimate value of grain size is around  $5.96\mu\text{m}$ . The presence of large grain may cause magnetic inhomogeneity to be reduced due to reduction of grain boundaries. As suggested by Mohan et al. [5], the enlargement of grain size favors the increase of volume of FM phase due to the reduction of magnetic inhomogeneity. Hence, in this study, the increased in sintering temperature is suggested to influence the growth of FM phase which attributed to the enlargement of grain size as consequences reduction in grain boundary density.



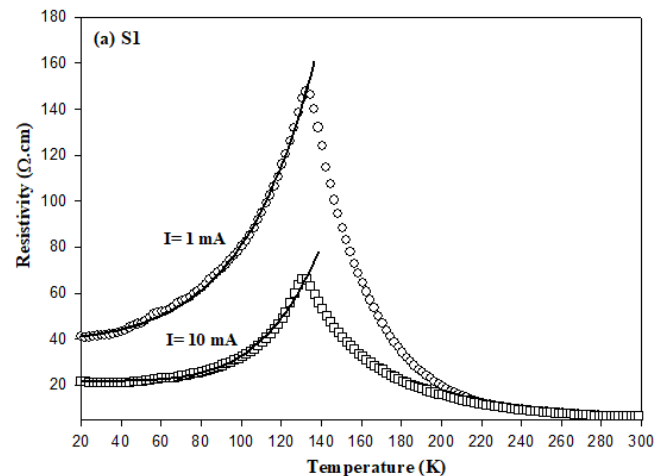
**Fig. 3:** Scanning Electron Micrograph with magnification of 10k for both samples, S1 (a) and S2 (b).

### 3.3. Electrical Properties

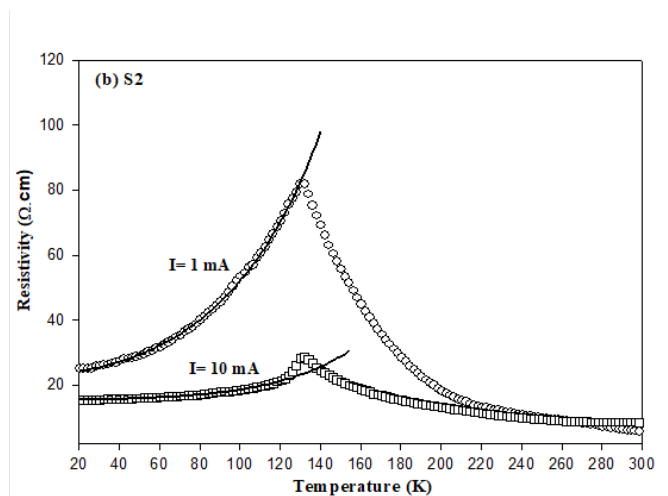
Fig. 4a and 4b show the resistivity – temperature ( $\rho$ - $T$ ) curve under different applied currents of 1 mA and 10 mA, in temperature range of 20 K to 300 K for both samples S1 and S2, respectively. From the graph, the sample exhibited metallic behavior at low-temperature region below metal-insulator transition temperature,  $T_{MI}$  and above the temperature, the sample exhibited insulating behavior. The resistivity peak in the  $\rho$  vs  $T$  curve was observed at the vicinity of  $T_{MI}$ . For sample S1 which sintered at  $TS = 1300^\circ\text{C}$ ,  $T_{MI}$  under applied current of 1 mA is 128.21 K, while the  $T_{MI}$  decreased to 120.58 K under applied current of 10 mA

For sample S2 which sintered at  $TS = 1400^\circ\text{C}$ ,  $T_{MI}$  under same applied current of 1 mA was found to be increased to 132.18 K compared with S1 sample, while  $T_{MI}$  under applied current of 10 mA was observed remained unchanged. The similar value of  $T_{MI}$  observed under both applied current was also reported by the Mohan et al. [5] in compound  $\text{Sm}_{0.55}\text{Sr}_{0.45}\text{MnO}_3$  which sintered at twice sintering processes at different temperatures. The increased

in  $T_{MI}$  for sample S2 indicates microstructure modification reduced magnetic inhomogeneity due to reduction of grain boundary density as a consequence the growth of ferromagnetic phase increase and, hence double exchange (DE) mechanism enhanced. The value of resistivity peak observed at the transition temperature,  $T_{MI}$  for sample S1 under applied current of 1 mA is  $422.53 \Omega \text{ cm}$ , while under applied current of 10 mA is  $147.82 \Omega \text{ cm}$ . It was found that the value of resistivity at the transition temperature,  $T_{MI}$  for sample S2 under applied current of 1 mA decreased to  $81.86 \Omega \text{ cm}$  compared with S1 sample, while under applied current of 10 mA, the resistivity drop to  $28.45 \Omega \text{ cm}$ . Similar observation in decreasing of resistivity peak value under same applied current was also reported by the Mohan et al. [5] in compound  $\text{Sm}_{0.55}\text{Sr}_{0.45}\text{MnO}_3$ . For both samples, the increased in applied current caused resistivity to drop, hence, conductivity increased which indicated that the number of charge carrier increased. The increased in charge carrier concentration is suggested due to applied electric field improved spin alignment of  $e_g$  of charge carrier, hence, DE mechanism enhanced. Under applied electric field, free charge carriers may have enough energy to overcome the insulating barrier at grain boundary region as consequences interfacial polarization process increased and, hence, decreased in resistivity as well as induced electroresistance (ER) effect as it is described in Fig. 5.



**Fig. 4a:** Resistivity–temperature plot of sample S1 ( $TS = 1300^\circ\text{C}$ ) under applied current of 1 mA and 10 mA, respectively. The solid lines show the fitting made to the equation  $\rho = \rho_0 + \rho_2 T^2 + \rho_5 T^5$



**Fig. 4b:** Resistivity–temperature plot of sample S2 ( $TS = 1400^\circ\text{C}$ ) under applied current of 1 mA and 10 mA, respectively. The solid lines show the fitting made to the equation  $\rho = \rho_0 + \rho_2 T^2 + \rho_5 T^5$

Fig. 5 describes the temperature dependence of electroresistance (ER %) for both samples S1 and S2. The ER, is defined as  $[\rho(I_1) - \rho(I_2)] / \rho(I_2) \times 100\%$  [5] where  $\rho(I_1)$  and  $\rho(I_2)$  are the resistivi-

ties of the sample at applied current of  $I_1 = 1\text{ mA}$  and  $I_2 = 10\text{ mA}$ , respectively. As shown in Fig. 5, for sample S2, ER maximum about 230 % is observed at the vicinity of  $T_{MI}$  while for sample S1, ER maximum is 140 % observed slightly below  $T_{MI}$ . The differences in ER maximum values for both samples, S1 and S2 may relate to the microstructure modification. Sample S1 which has smaller grain size compared to sample S2 showed smaller ER effect around  $T_{MI}$  compared to S2 sample. The findings showed that the increased in grain size enhanced the ER effect around  $T_{MI}$  which may relate to the formation of homogeneous grain as well as reduction in grain boundary density compared to sample S1, which influenced the resistance behavior. For sample S1, large grain boundary density may result to the increased in formation of magnetic inhomogeneity which was not much affected by the increased of applied current results in smaller change of resistivity at the vicinity of  $T_{MI}$  compared to sample S2 and as a consequence of smaller ER effect is observed for sample S1. For sample S2, it is suggested that the ordering of localized spins increased under increased of applied current and, hence, spin scattering of charge carrier reduced [9] which contribute to the large change of resistivity at the vicinity of  $T_{MI}$  and the observed large ER effect. The reduction of resistivity above  $T_{MI}$  in insulating region for both samples indicated increased in applied current enhanced the polarization of charge carrier at the grain boundaries region which may relate to the growth of FM phase and reduction of phase separated. The connectivity between FM cluster may form the percolative path for the currents to flow in insulating region and, hence, result in reduction of resistivity and the observation of ER effect [11].

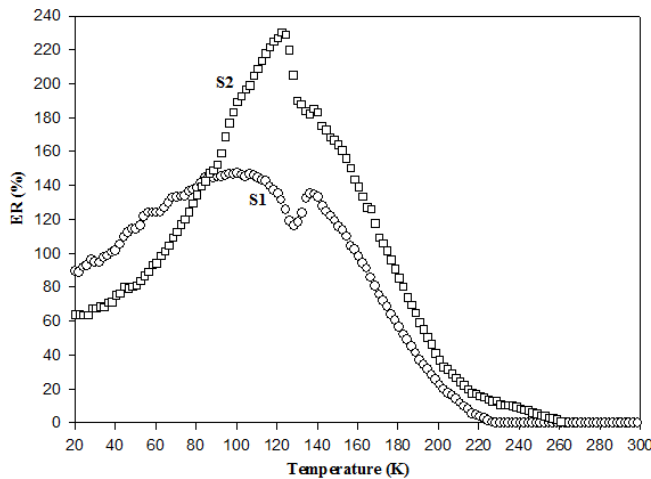


Fig. 5: Temperature dependence of electroresistance, ER for S1 and S2 samples.

The observed ER behaviour can be further understood by fitting the experimental resistivity data to the scattering models [12-14] in order to elucidate the possible mechanism involve for the-observed behavior. In the FM region below  $T_{MI}$ , the resistivity can be explained by the  $\rho = \rho_0 + \rho_2 T^2 + \rho_5 T^5$ . The first term of  $\rho_0$  represents the contribution of resistivity due to grain effect, while the second term of  $\rho_2 T^2$  represents the electron-electron scattering contribution to the resistivity and  $\rho_5 T^5$  represents the contribution to the resistivity due to electron-phonon scattering [13, 14]. As shown in Table 2, for both samples, the increased in applied current reduced the scattering effect as all the values of scattering parameter  $\rho_0$ ,  $\rho_2$  and  $\rho_5$  decreased with increased of applied current. The increased in applied current is found decreased in scattering effect caused the resistivity to decrease and, hence, induce the ER effect. In addition, the value of all parameters are smaller for sample S2 when compared with sample S1 suggested that scattering effect reduced as a result of grain modification. To understand the charge transport in insulating region above  $T_{MI}$ , the resistivity data was fitted using variable range hopping VRH model which represented by the empirical equation of  $\rho = \rho_0 \exp(T_0/T)^{1/4}$  [12-14]. Fig. 6a and 6b show the linear fitting of  $\ln \rho$

vs  $T^{-1/4}$  plots for both samples. As can be seen from Table 3, the hopping energy,  $E_h$  reduced with increased applied current which may relate to increase of delocalization of charge carrier due to less scattering effect and, hence, less energy is required for the hopping process.  $E_h$  is calculated based on the relation of  $E_h(T) = 1/4 k_B (T)^{3/4} (T_{om})^{1/4}$  where  $T_{om}$  is the Mott characteristic temperature and is related to carrier localization length which can be obtained from the slope of the graph of  $\ln \rho$  vs  $T^{-1/4}$  and  $k_B$  is Boltzmann's constant. Further,  $E_h$  was found to be significantly reduced for sample S2 which suggested enlarged in grain size further reduced the scattering effect and, hence, number of delocalization of charge carrier increased as shown by the increase of value of density of state at fermi level,  $N(E_F)$  in Table 3.  $N(E_F)$  was calculated using the equation of  $N(E_F) = 18 / k_B T_{om}$ , where  $\alpha$  is the localization length and the value of  $\alpha$  has been taken as 4.5 Å for the calculation to estimate the value of  $N(E_F)$  [13, 14].

Table 2: Best fitted parameters obtained from fitting experimental data in the metallic region to equations  $\rho = \rho_0 + \rho_2 T^2 + \rho_5 T^5$  of 1 mA and 10 mA for S1 and S2 samples.

Sample	$\rho_0 (\times 10^4) (\Omega \cdot \text{cm})$		$\rho_2 (\times 10^{-3}) (\Omega \cdot \text{cm} \cdot \text{K}^{-2})$		$\rho_5 (\times 10^{-9}) (\Omega \cdot \text{cm} \cdot \text{K}^{-5})$	
	$I = 1\text{ mA}$	$I = 10\text{ mA}$	$I = 1\text{ mA}$	$I = 10\text{ mA}$	$I = 1\text{ mA}$	$I = 10\text{ mA}$
S1	4.0083	2.1601	2.5000	0.2947	1.5548	1.0876
S2	2.3352	1.5354	2.3000	0.2000	0.5246	0.1140

Table 3: Best fitted parameters obtained from VRH model fitting under magnetic fields of 1 mA and 10 mA for S1 and S2 samples. The  $E_h$  and  $R_h$  values are calculated at  $T = 200\text{ K}$

Sample	$T_0 (\times 10^7 \text{ K})$		$E_h (200 \text{ K}) (\text{meV})$		$R_h (200 \text{ K}) (\times 10^{-2})$		$N(E_F) (\times 10^{23}) (\text{eV}^{-1} \cdot \text{cm}^{-3})$	
	$I = 1\text{ mA}$	$I = 10\text{ mA}$	$I = 1\text{ mA}$	$I = 10\text{ mA}$	$I = 1\text{ mA}$	$I = 10\text{ mA}$	$I = 1\text{ mA}$	$I = 10\text{ mA}$
S1	3.07	0.43	85.27	52.23	3.34	2.05	0.75	5.30
S2	0.60	0.03	56.71	25.63	2.22	1.00	3.81	91.38

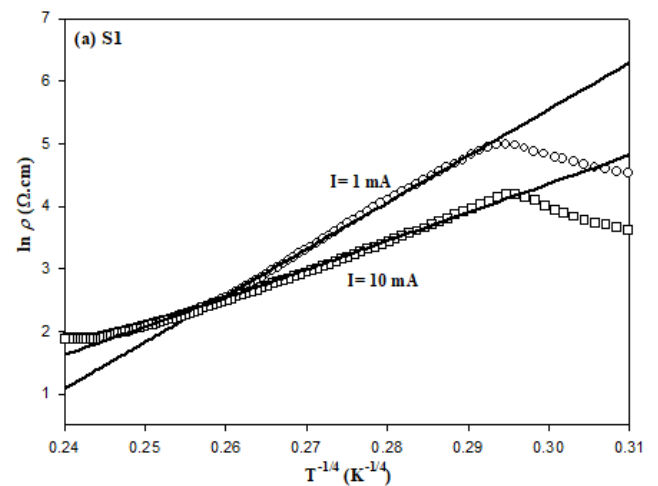
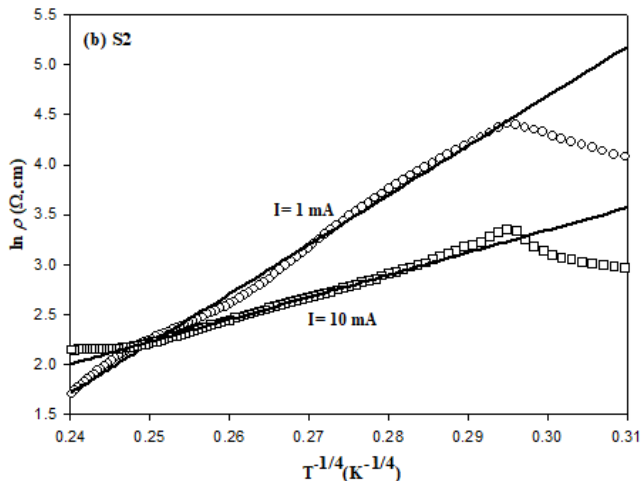


Fig. 6a: Resistivity-temperature plot of sample S1 ( $T_S = 1300^\circ\text{C}$ ) under applied current of 1 mA and 10 mA, respectively. The solid lines show the best fitting made to the small variable range hopping, VRH model.



**Fig. 6b:** Resistivity–temperature plot of sample S2 ( $T_S = 1400^\circ\text{C}$ ) under applied current of 1 mA and 10 mA, respectively. The solid lines show the best fitting made to the small variable range hopping, VRH model.

#### 4. Conclusion

The samples of  $\text{Sm}_{0.55}\text{Sr}_{0.45}\text{MnO}_3$  were prepared using solid state method which were sintered at different temperatures, which is at  $1300^\circ\text{C}$  (S1) and  $1400^\circ\text{C}$  (S2), respectively. It has been found that grain modification influenced the ER effect. Sample S2 with enlarged of grain size showed increased in ER maximum effect due to reduction of magnetic inhomogeneity in presence of increase of applied current. The effect of grain modification on the magnetic properties of sample has been studied by measuring AC magnetic susceptibility at temperature range from 40 K to 280 K. It has been found that grain modification does not much influence the magnetic properties as  $T_c$  remains almost constant for both samples, S1 and S2. The observed of enhanced ER effect at the vicinity of  $T_M$  may relate to the combination of reduction of scattering effect together with the improved in connectivity between ferromagnetic phase as a result of the enlargement of grain size for sample S2.

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